

**MOTOROLA**  
**SEMICONDUCTOR**  
**TECHNICAL DATA**

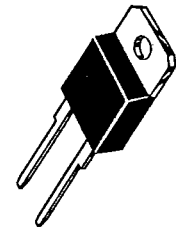
**Switchmode™**  
**Power Rectifier**

... designed for use in switching power supplies, inverters and as freewheeling diodes, these state-of-the-art devices have the following features:

- Ultrafast 85 ns (Typ) Soft Recovery Time @  $I_F = 1.0$  Amp,  $V_R = 30$  V,  $di/dt = 50$  A/ $\mu$ s
- 175°C Operating Junction Temperature
- State-of-the-Art Single TO-218 Plastic Package
- High Voltage Capability 1000 Volts
- Low Forward Voltage Drop
- Guaranteed Avalanche Energy Capability: 100 mJoules Min

**MUR30100E**

**ULTRAFAST  
RECTIFIER  
30 AMPERES  
1000 VOLTS**



**MAXIMUM RATINGS**

Rating	Symbol	Max	Unit
Peak Repetitive Reverse Voltage Working Peak Reverse Voltage DC Blocking Voltage	$V_{RRM}$ $V_{RWM}$ $V_R$	1000	Volts
Average Rectified Forward Current (Rated $V_R$ ) $T_C = 70^\circ\text{C}$	$I_{F(AV)}$	30	Amps
Peak Repetitive Forward Current (Rated $V_R$ , Square Wave, 20 kHz) $T_C = 150^\circ\text{C}$	$I_{FRM}$	30	Amps
Non-Repetitive Peak Surge Current (Surge applied at rated load conditions halfwave, single phase, 60 Hz)	$I_{FSM}$	300	Amps
Operating Junction Temperature	$T_J$	-65 to +175	°C
Storage Temperature	$T_{stg}$	-65 to +175	°C

**THERMAL CHARACTERISTICS**

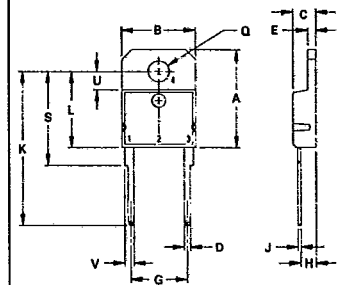
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1.4	°C/W
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**ELECTRICAL CHARACTERISTICS**

Characteristic	Symbol	Max	Min	Unit
Instantaneous Forward Voltage (1) ① $I_F = 30$ Amps, $T_C = 25^\circ\text{C}$ ② $I_F = 30$ Amps, $T_C = 100^\circ\text{C}$	$V_F$	1.9 1.8	—	Volts
Instantaneous Reverse Current (1) ① Rated DC Voltage, $T_C = 25^\circ\text{C}$ ② Rated DC Voltage, $T_C = 100^\circ\text{C}$	$I_R$	100 5.0	—	$\mu$ A mA
Reverse Recovery Time $I_F = 1.0$ Amp, $V_R = 30$ V, $di/dt = 50$ A/ $\mu$ s	$t_{RR}$	100	—	ns
Controlled Avalanche Energy	$W_{(aval)}$	—	100	mJ

SWITCHMODE is a trademark of Motorola Inc.

**OUTLINE DIMENSIONS**



NOTES:  
1. DIMENSION A, G AND TOLERANCING PER ANSI Y14.5M, 1987  
2. CONTROLLING DIMENSION: MILLIMETER

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	19.00	19.60	0.749	0.771
B	14.00	14.50	0.551	0.570
C	4.20	5.00	0.165	0.196
D	1.00	1.30	0.040	0.051
E	1.45	1.65	0.058	0.064
G	10.42	11.44	0.411	0.450
H	2.60	3.00	0.103	0.118
J	0.40	0.60	0.016	0.023
K	28.50	32.00	1.122	1.259
L	14.73	15.50	0.579	0.607
Q	4.00	4.25	0.158	0.167
S	17.50	19.50	0.689	0.767
U	3.40	3.80	0.134	0.149
V	1.50	2.00	0.060	0.078

STYLE 1  
PIN 1 CATHODE  
3 ANODE  
4 CATHODE

**CASE 340E-01  
TO-218**



**MOTOROLA**

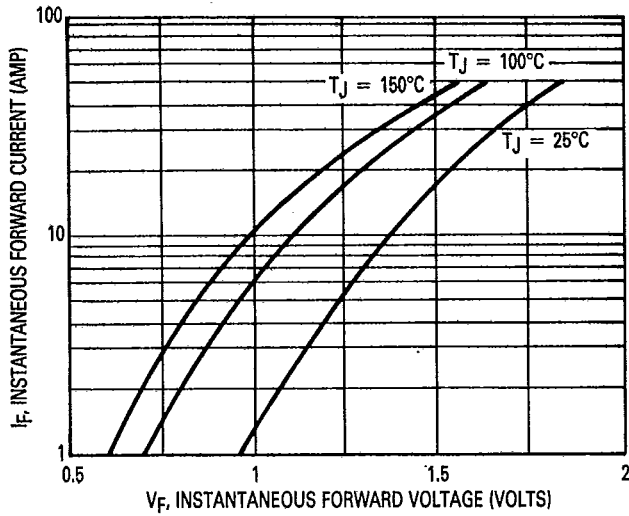


Figure 1. Typical Forward Voltage

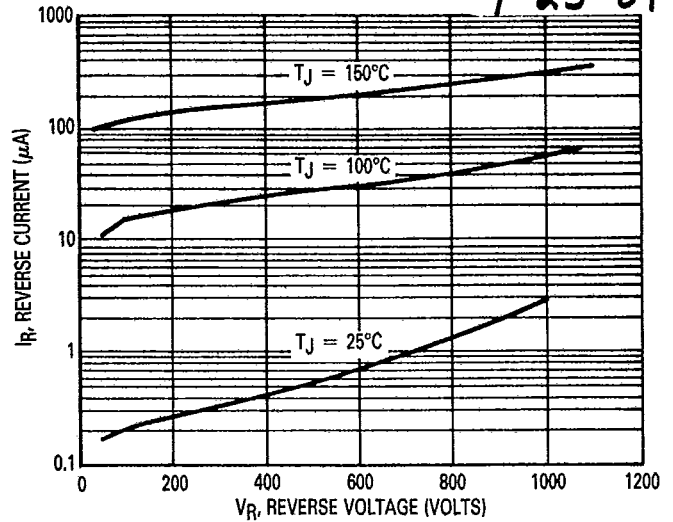


Figure 2. Typical Reverse Current

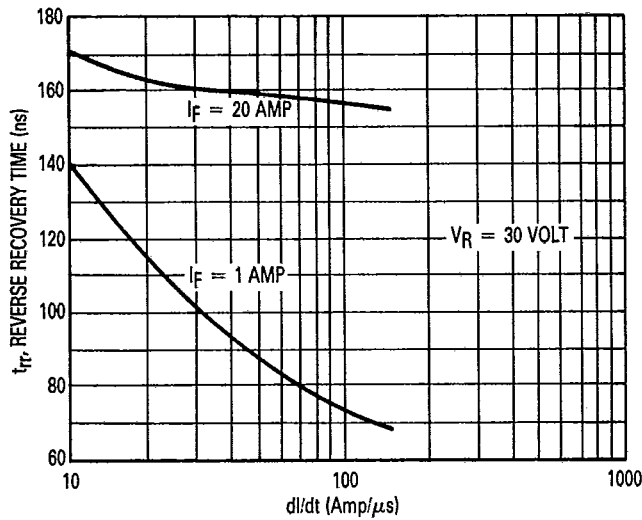


Figure 3.  $t_{rr} = f(dI/dt)$  at  $T_J = 25^\circ\text{C}$

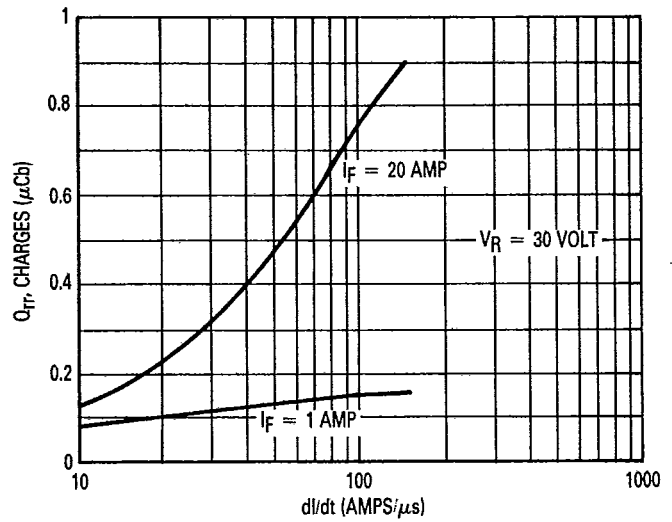


Figure 4.  $Q_{rr} = f(dI/dt)$  at  $T_J = 25^\circ\text{C}$

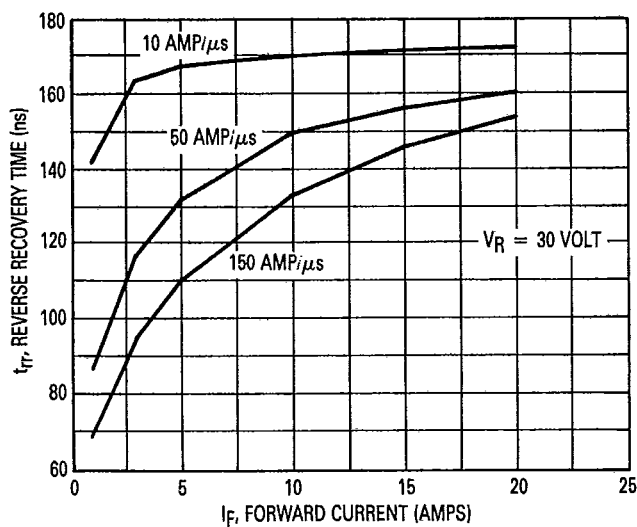


Figure 5.  $t_{rr} = f(I_F)$  at  $T_J = 25^\circ\text{C}$

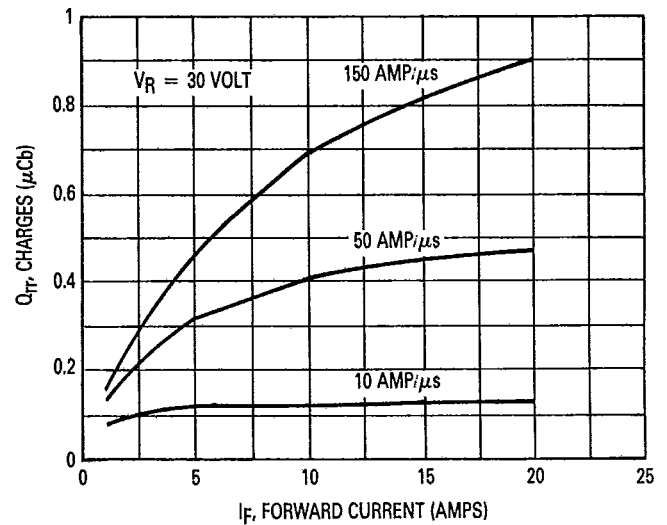


Figure 6.  $Q_{rr} = f(I_F)$  at  $T_J = 25^\circ\text{C}$

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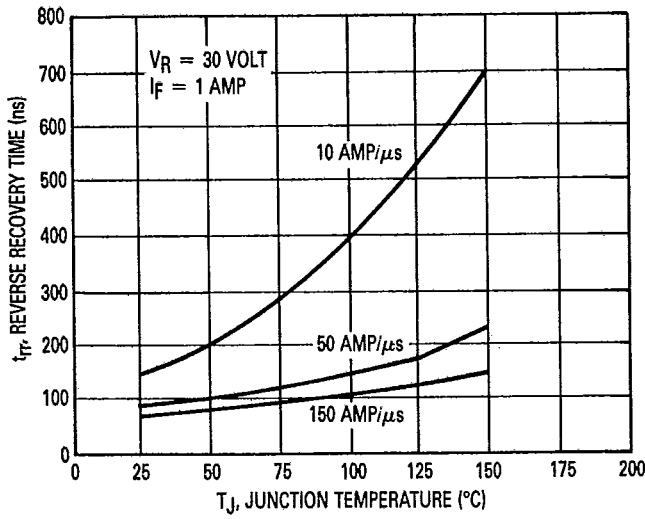


Figure 7.  $t_{rr} = f(T_J)$

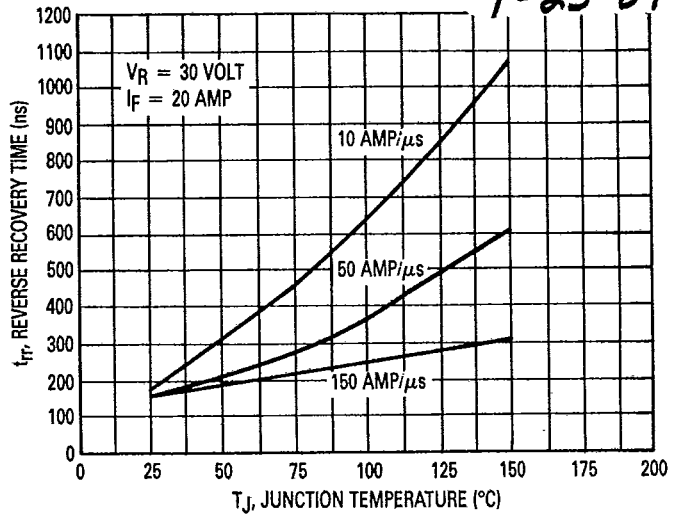


Figure 8.  $t_{rr} = f(T_J)$

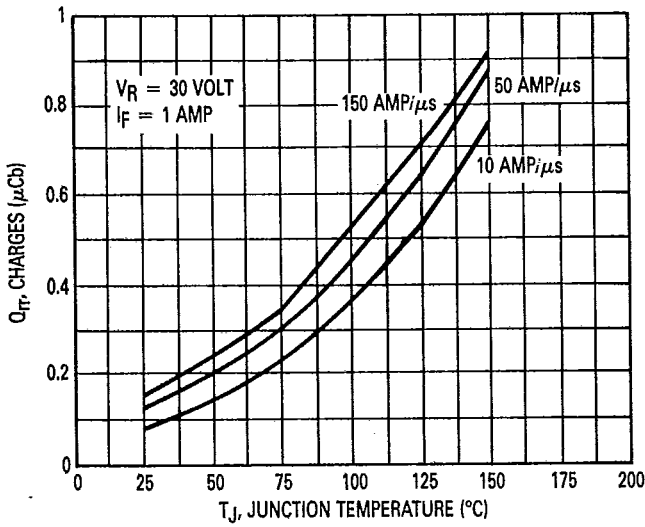


Figure 9.  $Q_{rr} = f(T_J)$

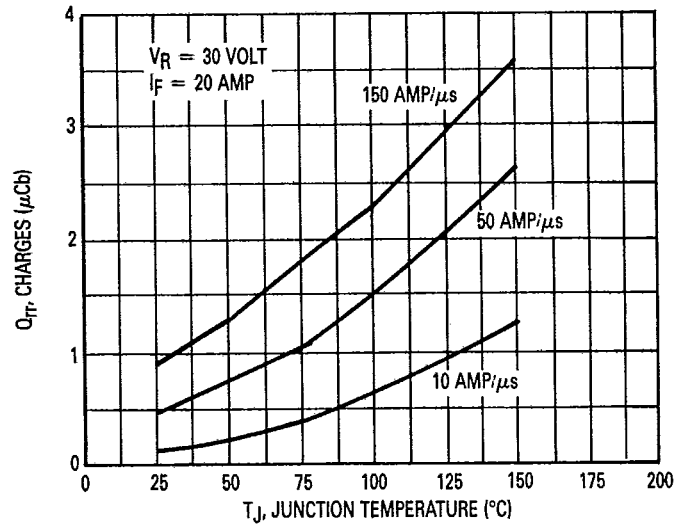


Figure 10.  $Q_{rr} = f(T_J)$

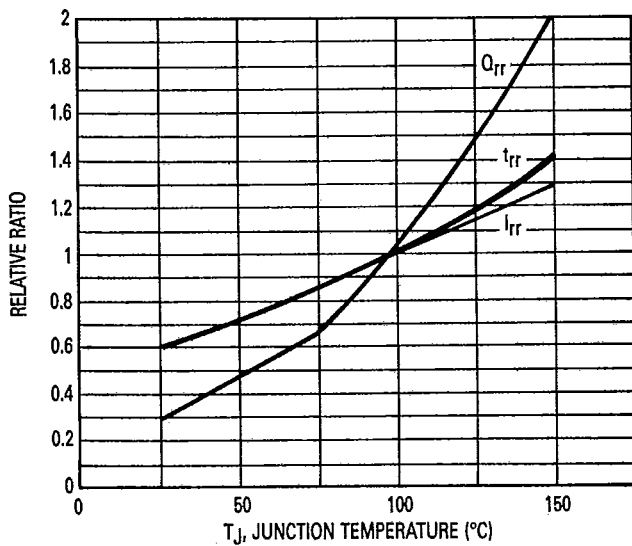
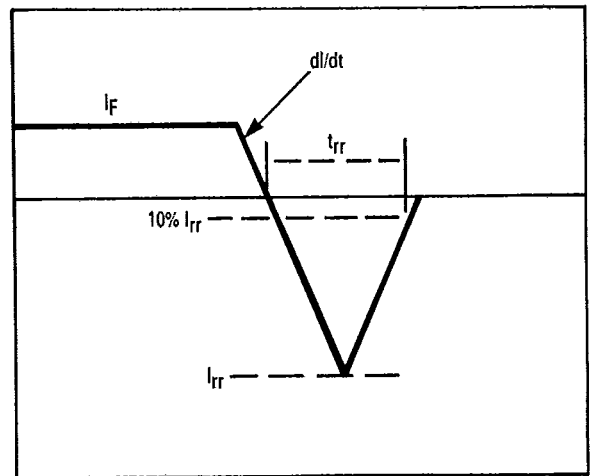


Figure 11. Dynamic Parameters =  $f(T_J)$



$t_{rr}$ : lapse between  $I_F$  crossing the 0 axis downward and  $I_R$  reaching 10% of  $I_{rr}$  upward

Figure 12.  $t_{rr}$  Definition

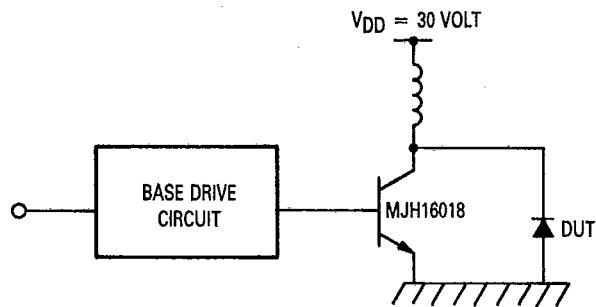


Figure 13. Avalanche Test Circuit

The unclamped inductive switching circuit shown in Figure 13 was used to demonstrate the controlled avalanche capability of the new "E" series Ultrafast Rectifiers. Figure 14 represents the Current-Voltage waveforms during tests.

When the transistor is turned-on at  $t_0$ , the current in the inductor  $I_L$  ramps up linearly and energy is stored in the coil. At  $t_1$  the transistor is turned-off and voltage across the diode under test begins to rise rapidly due to  $di/dt$  effects. When this induced voltage reaches the breakdown voltage of the diode, it is clamped at  $BV(DUT)$  and the diode begins to conduct the full load current which now starts to decay linearly through the diode and goes to zero at  $t_2$ .

By solving the loop equation at the point in time when the transistor is turned-off, and calculating the energy that is transferred to the diode, it can be shown that the total energy transferred is equal to the energy stored in the inductor plus a finite amount of energy from the  $V_{DD}$  power supply while the diode is in breakdown (from  $t_1$

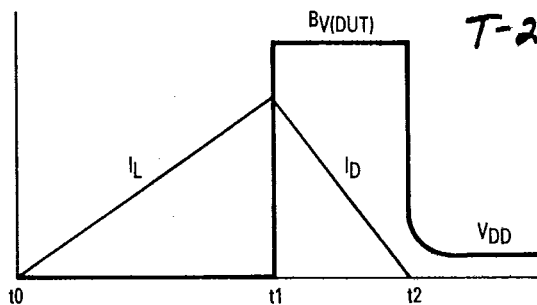


Figure 14. Current-Voltage Waveforms

to  $t_2$ ), minus any losses due to finite component resistances.

Assuming the component resistive elements are small, Equation 1 approximates the total energy transferred to the diode. It can be seen from this equation that if the  $V_{DD}$  voltage is low compared to the breakdown voltage of the DUT, the amount of energy contributed by the supply during breakdown is small and the total energy can be assumed to be nearly equal to the energy stored in the coil during the time the transistor was ON, Equation 2.

Although it is not recommended to design for this condition, the new "E" series provides added protection against those unforeseen transient viruses that can produce unexplained random failures in unfriendly environments.

**EQUATION 1:**

$$W_{aval} = 1/2 LI^2(peak) (BV(DUT)/(BV(DUT) - V_{DD}))$$

**EQUATION 2:**

$$W_{aval} = 1/2 LI^2(peak)$$

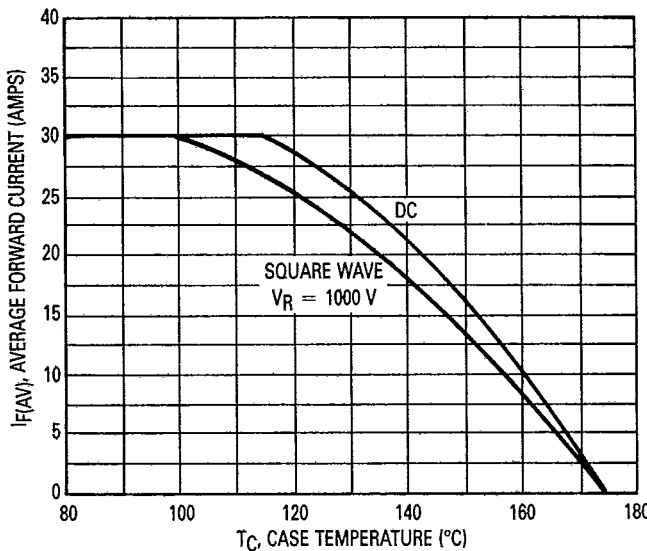


Figure 15. Current Derating, Case

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