TOSHIBA BiCD Digital Integrated Circuit Silicon Monolithic

TB62731FU

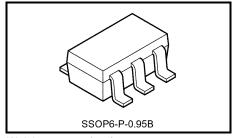
Step-up DC-DC Converter for White LED Driver

The TB62731FU is an LED driver which uses a high power efficiency step-up DC-DC converter. The converter turns on/off from 2 to 6 white LEDs in series.

The IC incorporates an N-channel MOSFET transistor which switches a coil. Also, a function which reduces LED current depending on increase in temperature.

The mean LED current can be easily set using an external resistor.

The IC is ideal as a driver for LED light sources used as liquid crystal backlights for PDAs, cellular phones, and handy terminals.



Weight: 0.016 g (typ.)

Features

- Maximum output voltage: Vo ≤ 28 V
- Mean LED current values set according to external resistor

14 mA (typ.) @R_sens = 2.7Ω

20 mA (typ.) @R_sens = 1.8Ω

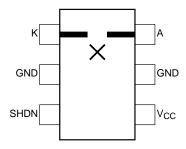
- Supply power: Up to 320 mW supported
- Compact package: SSOP6-P-0.95B, 6 pins
- · Built-in temperature derating function: LED current derated automatically depending on temperature
- High power efficiency

Up to 80% of peak power efficiency achieved using recommended components

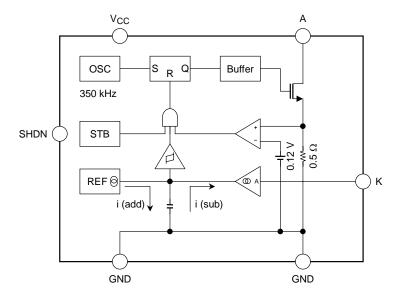
Ron = 2.0Ω (typ.) @VIN = $3.2 \sim 5.5 \text{ V}$

Built-in low Ron power MOS switch

Pin assignment (top view)



Block Diagram



Pin Functions

No	Symbol	Function
1	К	Pin connecting LED cathode to resistor used to set current. Feedback pin for voltage waveforms for controlling LED constant current.
2, 5	GND	Ground pin for logic
3	SHDN	IC enable pin. When Low, Standby Mode and pin A turned off.
4	V _{CC}	Input pin for power supply for operating the IC. Operating voltage range: 3.0~5.5 V
6	Α	DC-DC converter switch pin. The switch is an N-channel MOSFET transistor.

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Note: Connect both GND pins to ground.

Absolute Maximum Ratings (unless otherwise specified, $T_{opr} = 25$ °C)

Characteristics	Symbol	Rating	Unit	
Supply voltage	V _{CC}	-0.3~+6.0	V	
Input voltage	V _{IN}	-0.3~+V _{CC} + 0.3	V	
Pin A (anode) current	I _o (A)	+270	mA	
Pin A voltage	V _o (A)	-0.3~+28	V	
		0.41 (IC only)		
Power dissipation	P _D	0.47 (IC mounted on PCB) (Note)	W	
Saturation thermal resistance	R _{th (j-a)} 1	300 (IC only)	°C/W	
Saturation thermal resistance	R _{th (j-a)} 2	260 (IC mounted on PCB)	C/VV	
Operating temperature range	T _{opr}	-40~+85	°C	
Storage temperature range	T _{stg}	-40~+150	°C	
Maximum junction temperature	Tj	125	°C	

Note: Derate power dissipation by 3.8 mW/°C from the Absolute maximum rating for every 1°C exceeding the ambient temperature of 25°C (when IC is mounted on PCB).

Recommended Operating Conditions (unless otherwise specified, $T_{opr} = -40 \sim 85$ °C)

Characteristics	Symbol	Test circuit	Test condition	Min	Тур.	Max	Unit
Supply voltage	V _{CC}	_	_	3.0	_	4.3	V
SHDN pin high-level input voltage	V _{IH}	_	_	V _{CC} - 0.5	_	V _{CC}	٧
SHDN pin low-level input voltage	V _{IL}	_	_	0	_	0.5	V
SHDN pin high-level input pulse width	tpw SHDN	_	_	500	_	_	μS
Set LED current (mean)	l _o	_	$V_{o}(A) = V_{IN} 3.0 \text{ V}, V_{OUT} 16 \text{ V}$	5		20	mA

Electrical Characteristics (unless otherwise specified, $Ta = -40 \sim 85$ °C, $V_{CC} = 3.0 \sim 5.5$ V)

Characteristics	Symbol	Test circuit	Test condition	Min	Тур.	Max	Unit
Supply voltage	V _{CC}	_	_	3.0	_	5.5	V
Current consumption at operation	I _{CC} (ON)	_	V _{CC} = 3.6 V		0.6	0.9	mA
Current consumption at standby	I _{CC} (SHDN)	_	SHDN = 0 V	_	0.5	1.0	μА
SHDN pin current	I_SHDN	_	SHDN = V _{CC} , Built-in pull-down resistor	_	4.2	7	μА
Internal MOS transistor on-resistance	Ron	_	I (A) ≦ 270 mA, Including detected resistance	_	2.0	2.5	Ω
Internal MOS transistor switching frequency	fosc	_	_	275	350	425	kHz
Pin A voltage	V _o (A)	_	_	28	_	_	V
Pin A current	I _o (A)	_	_	210	240	270	mA
Pin A leakage current	I _{oz} (A)	_	_		0.5	1	μА
Set LED current (mean)	Io	_	$V_{CC} = 3.2 \sim 4.2 \text{ V},$ $R_{sens} = 1.8 \Omega$ $T_{opr} = 25 ^{\circ}C$ (Note 1)	17.6	20	22.4	mA
Pin K derating start ambient temperature	Tdel	_	Equivalent to R_sens = 1.8 Ω , L = 4.7 μ H, V ₀ = 16 V	_	45 (Note 2)	_	°C

Note 1: Because the temperature derating function operates, measure when Ta = 25°C.

Note that fluctuation in R_sens resistors is not included in the specified value.

Io may be different from the specified value due to the relation between the inductor value and load.

Note 2: Guaranteed by design

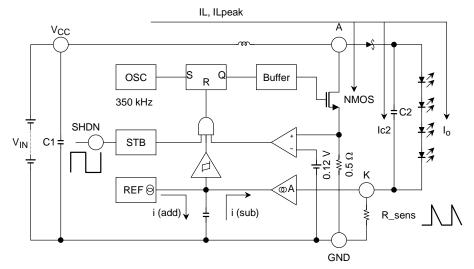


Figure 1 Application Circuit

The basic TB62731FU circuit uses a step-up DC-DC converter and burst control of current pulse.

Basic Operation

The internal MOS transistor (NMOS) is turned on at fOSC = 350 kHz, charging energy to the inductor. Inductance current IL increases from 0. When IL = ILpeak = 240 mA (typ.) or when 5/6 (83.3%) of fOSC (= 350 kHz) is reached, the transistor is turned off.

At that time, the coil maintains IL = ILpeak, the Schottky diode is turned on, and IL = Ic2 flows. Then, Ic2 decreases, reaching IL = 0.

The above operation repeats. When Ic2 is fully charged, the surplus current becomes I_0 , which flows to the LED.

The graph below shows details of the basic pulse used for burst control.

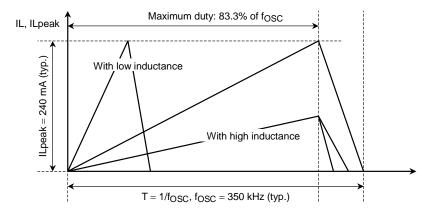


Figure 2 Switching Waveform of Inductance

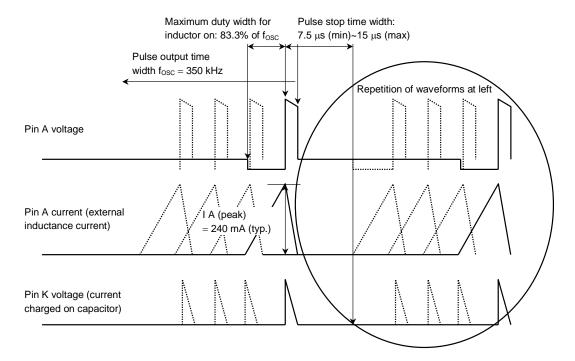


Figure 3 Burst Control Waveforms

Burst Control

Burst control is control of the number of current pulses, shown in the graph on the previous page. Control is repeated in desired cycles. The current pulse in the graph is the charged current on capacitor 2 (C2) for output.

The current pulse is supplied to the LED as current discharged from the output-side capacitor. The current pulse flows to GND via R_sens.

The waveform of the voltage charged on the output-side capacitor is fed back to the IC from pin K via C2.

The internal circuit which uses pin K for input controls the number of current pulses so that the mean voltage value of the obtained voltage waveform is 36 mV. As a result, the output current is controlled as the constant current (= mean current).

Connecting R_sens = 1.8Ω obtains the mean current ($36 \text{ mV} \div 1.8 \Omega = 20 \text{ mA}$).

Current is controlled by PFM (pulse frequency modulation) because the time when the output pulse is generated varies (increases/decreases).

A prerequisite is that the input power from V_{IN} is larger than the output power to the LED load. The constant current is maintained by fixing a pulse stop time of $7.5\sim15~\mu s$ and increasing/decreasing the number of current pulses. When the input power is more than the output power, the number of current pulses is fewer; when less, the number of pulses is larger.

The burst frequency (pulse generation frequency) at controlled constant current is calculated as follows: fburst [Hz] = (number of current pulses x $(1/275\sim1/350 \text{ kHz})$ + pulse stop time $(7.5\sim15 \text{ }\mu\text{s})$. . . formula 1

The IC is designed to supply a load power of 320 mW (min).

Generally, a step-up inductance of $47 \,\mu H$ is used for optimum design for the load power of 320 mW. When the load power is small, the inductance must be small.

Make sure the following condition for LED load between pins A and K is satisfied.

V_{IN} (V_{CC}) < LED Vf total

Note that, regardless of control by the IC, LEDs are always on.

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Standby Operation

The SHDN pin is used to set normal or standby operation. When SHDN is set to Low, the operation is standby; when High, the LED is turned on. Current consumption in Standby Mode is $1 \mu A$ (max).

Output-side capacitor setting

When the output-side capacitor (C2) = $0.1~\mu F$, the peak current to be supplied to LEDs is expected to be the set current $+5 \sim +8~mA$.

When $C2 = 0.01~\mu\text{F}$, the peak current is expected to be the set current +20~30 mA. When $C2 = 1~\mu\text{F}$, the set current +2~3 mA. Toshiba recommend $C2 = 1~\mu\text{F}$ or more considering the LED max If.

The IC is used only for lighting LEDs. The IC does not finely control output current ripples, because eliminating ripples is considered unnecessary as the LED emittance is recognized as the integral amount.

External inductance setting

The minimum external inductance is calculated as follows:

```
L(\mu H) = ((K \times P_0) - V_{IN} \min \times I_0) \times (1/f_{OSC} \min) \times 2 \times (1/I_{ID} \min \times I_{ID} \min) \dots formula 2
```

The above parameters are described below:

Po: output power (power required by LED load)

 P_0 (W) = Vf LED × If LED + Vf schottky × If LED + R_sens × If LED × If LED

LED forward current: If LED (mA) = Set current: Io (mA), LED forward voltage: Vf LED (V),

Schottky diode forward voltage: Vf schottky (V),

Setting resistance: $R_{sens}(\Omega)$

VIN min (V): minimum input voltage (battery voltage)

If the input voltage includes a resistance component, take the voltage drop into consideration for the minimum input voltage.

The input current IIN is roughly estimated as follows:

$$I_{IN}$$
 (mA) = VfLED × I_0 × (1/ η) × (1/ V_{IN}) . . . formula 3

When min V_{IN} = 3.2 (V), VfLED = 16 (V), I_0 = 18 (mA), and $\eta \ge 75$ (%), then I_{IN} = 0.12 (mA). As a result, the voltage drops by 1.2 V due to the 1- Ω DC resistance component. Because the IC's minimum V_{CC} = 3.0 V, the minimum V_{IN} is 3.12 V ($V_{IN} \ge 3.12$ V).

 I_0 (A): Mean current value set according to resistance R_sens (Ω)

fosc (Hz): Switching frequency of internal MOS transistor

Specified values for fosc (kHz): 275 min, 350 typ., 475 max

Ip (A): Peak current value supplied to external inductor

Specified values for Ip (A): 230 min, 240 typ., 270 max

K: Margin of output power $K = 1.1 \sim 1.3$

The ideal condition is to give 1.05 to 1.3 times the output power P_0 as the input power.

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The loss of the IC is assumed to be included in the margin.

If K is too large, it may not be possible for the current characteristic to be the specified value. Note that K > 1.

Substitute the following conditions in formula 2.

Supply voltage $V_{IN} = 3.0 \sim 4.3$ (V)

Output-side capacitor C2 = 1 (μF) . . . C2 is ignored in the calculation.

Where it is assumed that,

VfLED = 16 (V), Vf schottky = 0.3 (V), R_sens = 1.8 (Ω), $I_0 = 20$ (mA), K = 1.1

VfLED: LED Vf

 $Vf\ schottky\hbox{:}\ Schottky\ diode\ Vf$

R_sens: setting resistance

 I_0 : set current K: margin

$$L \; (\mu H) = ((1.1 \times 16 \times 0.02) - 3 \times 0.02) \times (1/275e3) \times 2 \times (1/(0.21 \times 0.21)) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V) \\ 43.8 \; (\mu H, \, V_{IN} = 4.3 \; V) + (1/275e3) \times 2 \times (1/(0.21 \times 0.21)) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V) + (1/275e3) \times 2 \times (1/(0.21 \times 0.21)) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V) + (1/275e3) \times 2 \times (1/(0.21 \times 0.21)) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V) + (1/275e3) \times 2 \times (1/(0.21 \times 0.21)) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V) + (1/275e3) \times 2 \times (1/(0.21 \times 0.21)) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V) + (1/275e3) \times 2 \times (1/(0.21 \times 0.21)) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V) + (1/275e3) \times 2 \times (1/(0.21 \times 0.21)) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V) + (1/275e3) \times 2 \times (1/(0.21 \times 0.21)) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V) + (1/275e3) \times 2 \times (1/(0.21 \times 0.21)) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V) + (1/275e3) \times 2 \times (1/(0.21 \times 0.21)) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V) + (1/275e3) \times 2 \times (1/(0.21 \times 0.21)) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V) + (1/275e3) \times (1/275e3) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V) + (1/275e3) = \; 48.1 \; (\mu H, \, V_{IN} = 3.0 \; V)$$

Thus, 48.1 (µH) is selected when the input voltage is low, 3.0 V.

Note that the calculation does not consider fluctuations in inductance. To shiba recommend selection of an inductance of 1.2 times the calculated value.

The recommended inductance under the above conditions is L (μ H) = 48.1 (μ H) × 1.2 \geq 57.7 (μ H).

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Selection of R_sens

Resistance between pin K and GND R_sens (Ω) is used for setting output current I_0 . The mean output current I_0 can be set according to the resistance.

The mean current I_0 (mA) to be set is roughly calculated as follows:

 I_0 (mA) = 36 (mV) ÷ R_sens (Ω)

For example, when $R_sens = 1.8 (\Omega)$, $I_0 = 20 (mA)$.

Take a current error of ±10% (not including R_sens error) into consideration.

The IC has a minimum output $P_0 = 320$ (mA, choke coil = 47 μ H).

At that time, if the product of mean current I_0 and output voltage V_0 exceeds P_0 = 320 (mW), mean current I_0 may become less than the desired value.

If the IC is not connected to the output-side capacitor (for smoothing), set current Io can be obtained.

At that time, because the current which flows to the LED is a pulse current with a maximum peak value of 270 mA, make sure that surge current IFP (mA) does not flow to the LED.

Toshiba recommend use of components with low reactance (parasitic inductance) and minimized PCB wiring. Toshiba also recommend allocating components in the application circuit diagram as near each other as possible.

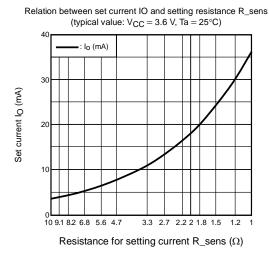


Figure 4

Output Derating Function

To shiba recommend derating LED current depending on the increase in ambient temperature. TB62731FU is intended to safely and efficiently drive white LEDs used as backlight sources for color LCDs. The IC incorporates a function which derates current based on the set temperature (the ambient temperature when the IC is mounted), Ta.

The IC features an output current which varies according to the internally-detected temperature T_{js} as follows: when T_{js} = 45 (°C), output current is 100%; when T_{js} = 100 (°C), output current is 0%.

The derating start temperature T_s (°C) is determined based on T_a ($T_a = T_s$ when the IC is not operating) by subtracting the self-generated temperature T_{up} (°C) from $T_{is} = 45$ (°C).

```
T_{s} (°C) = 45 (°C) – T_{up} (°C) . . . formula 4
```

The derating characteristic is as shown in the graph below (Figure 5). Figure 5 shows the relation between output current change ratio and internally-detected temperature (IC temperature) T_{is}.

The self-generated temperature T_{up} (°C) is calculated as follows:

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T_{up} (°C) = (P loss (W) – P parts (W)) × \theta_{ja} (°C/W) ) . . . formula 5
```

P loss: power loss

P parts: power loss of parts

 θ_{ja} : package saturation thermal resistance (Ω)

The parameters are described below:

DC resistance of inductor: RDC (Ω)

LED forward current: If LED (A)

LED forward voltage: Vf LED (V)

Schottky diode forward voltage: Vf schottky (V)

Setting resistance: R_sens

```
P loss (W) \simeq P_0 (W) \div \eta (\%) - P_0 (W)
```

Po: output power

η: power efficiency

P parts (W) \simeq RDC \times IIN + Vf schottky \times If LED + R_sens \times If LED \times If LED

 θ_{ja} (°C/W) ≤ 260 (°C/W)

max when IC mounted on PCB

 $P_0(W) = V_0(V) \times I_0(A)$

Vo: Vf LED output voltage

 I_0 : mean output current = set current

 $P_i(W) = V_{IN}(V) \times I_{IN}(A)$

Pi: input power

VIN: input voltage

IIN: mean input current

$$\eta$$
 (%) = 100 × P₀ (W) ÷ P_i (W)

Example of calculation: Where the measurement result for any lighting circuit shows the following values: RDC = 0.5 (Ω), P_0 = 320 (mW), I_{IN} = 0.1 (mA), I_0 = 20 (mA), R_s ens = 1.8 (Ω), Vf schottky = 0.3 (V), and η = 70 (%)

The self-generated temperature $T_{\rm up}$ (°C) is calculated as follows:

$$T_{up} \ (^{\circ}C) = ((0.32 - (0.32 \times 0.7)) - (0.5 \times 0.1 + 0.3 \times 0.02 + 1.8 \times 0.02 \times 0.02)) \times 260 = 10.2 \ (^{\circ}C) = (0.32 - (0.32 \times 0.7)) - (0.5 \times 0.1 + 0.3 \times 0.02 + 1.8 \times 0.02 \times 0.02)) \times 260 = 10.2 \ (^{\circ}C) = (0.32 \times 0.7) \times 0.02 \times 0.02) \times 0.02 \times 0.02 \times 0.02 \times 0.02 \times 0.02)$$

Thus, the derating start temperature T_s (°C) is calculated as follows:

$$T_s$$
 (°C) = 45 (°C) – 10.4 (°C) = 34.8 (°C)

As a result, I_0 is controlled in the recommended current range as shown in Figure 5.

Because saturation thermal resistance θ_{ja} = 260 (°C/W) is the maximum value, θ_{ja} = 210~260 (°C/W) is used as a mounting condition.

Depending on the IC characteristics, peripherals, and use environment, the derating start temperature fluctuates among ICs.

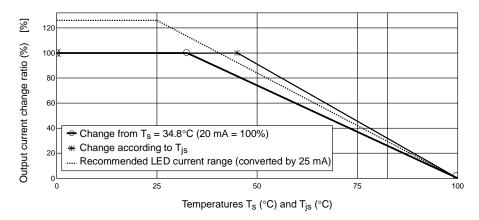
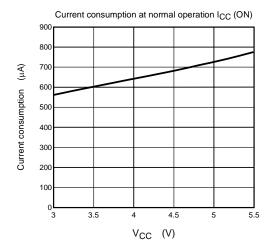
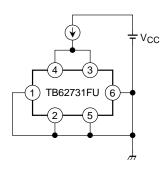
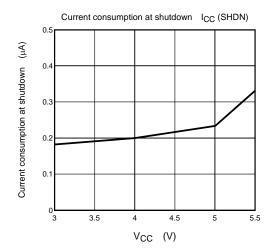
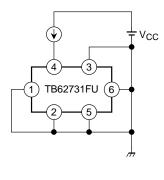


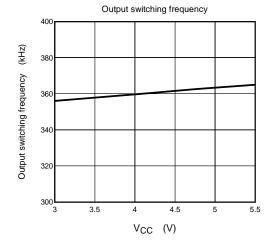
Figure 5 Derating Function of Set Current

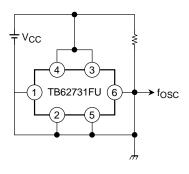






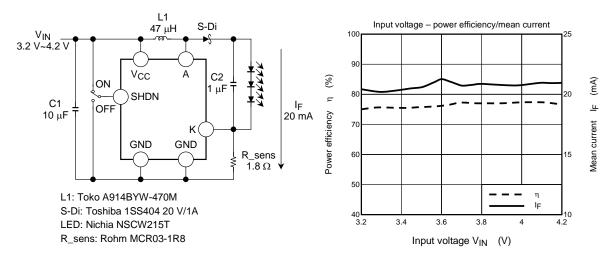


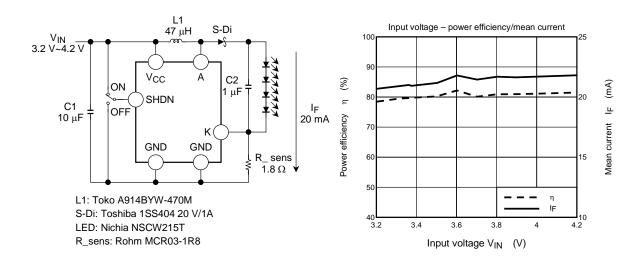


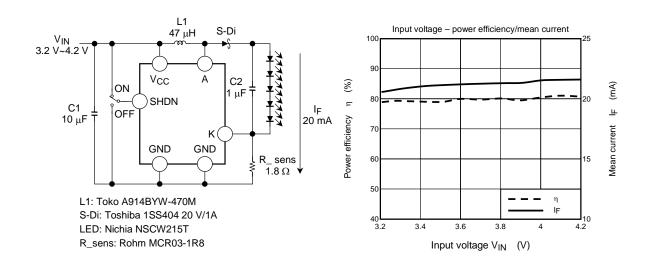


Application Circuit Example 1 (characteristic using recommended coil as reference)

Though it is necessary to consider the DC resistance of L1, an inductance of 33 to 47 (typ.) to 68 μ H is suitable for turning on four LEDs.

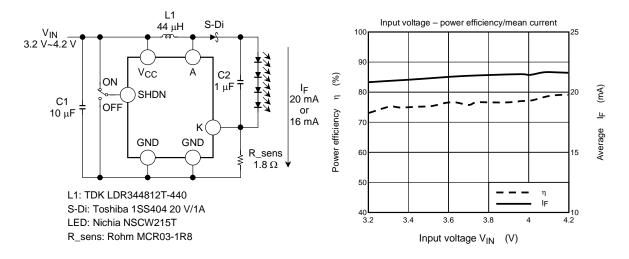


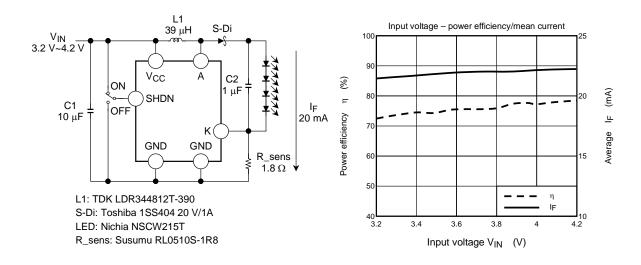


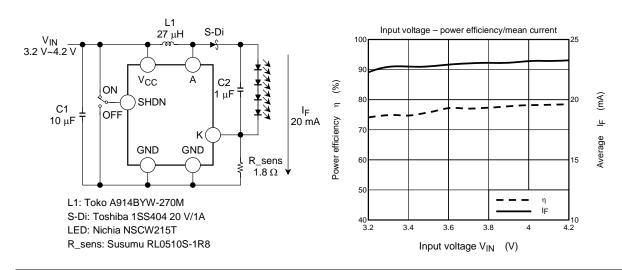


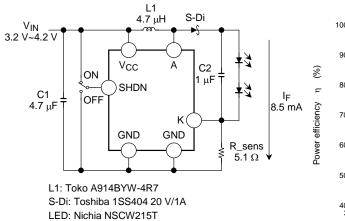
Application Circuit Example 2 (characteristic using flat coil for handy terminal as reference)

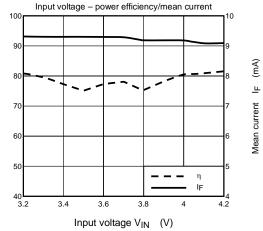
Flat coils suitable for handy terminals have a large DC resistance; thus, the power efficiency drops slightly, to about 70%.

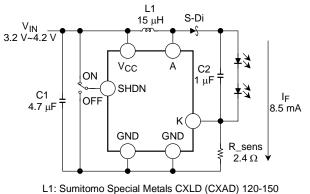


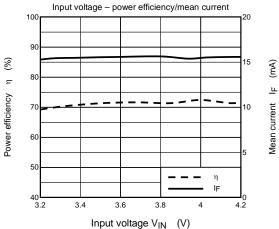












L1: Sumitomo Special Metals CX S-Di: Toshiba 1SS404 20 V/1A LED: Nichia NSCW215T

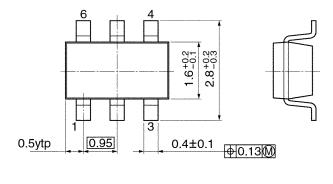
R_sens: —

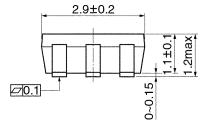
R_sens: ---

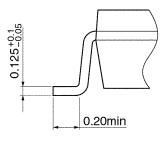
Package Dimensions

SSOP6-P-0.95B

Unit: mm







Weight: 0.016 g (typ.)

Notes on Contents

1. Block Diagrams

Some of the functional blocks, circuits, or constants in the block diagram may be omitted or simplified for explanatory purposes.

2. Equivalent Circuits

The equivalent circuit diagrams may be simplified or some parts of them may be omitted for explanatory purposes.

3. Timing Charts

Timing charts may be simplified for explanatory purposes.

4. Application Circuits

The application circuits shown in this document are provided for reference purposes only.

Thorough evaluation is required, especially at the mass production design stage.

To shiba does not grant any license to any industrial property rights by providing these examples of application circuits.

5. Test Circuits

Components in the test circuits are used only to obtain and confirm the device characteristics. These components and circuits are not guaranteed to prevent malfunction or failure from occurring in the application equipment.

IC Usage Considerations

Notes on Handling of ICs

(1) The absolute maximum ratings of a semiconductor device are a set of ratings that must not be exceeded, even for a moment. Do not exceed any of these ratings.
Exceeding the rating(s) may cause the device breakdown, damage or deterioration, and may result injury by explosion or combustion.

- (2) Use an appropriate power supply fuse to ensure that a large current does not continuously flow in case of over current and/or IC failure. The IC will fully break down when used under conditions that exceed its absolute maximum ratings, when the wiring is routed improperly or when an abnormal pulse noise occurs from the wiring or load, causing a large current to continuously flow and the breakdown can lead smoke or ignition. To minimize the effects of the flow of a large current in case of breakdown, appropriate settings, such as fuse capacity, fusing time and insertion circuit location, are required.
- (3) If your design includes an inductive load such as a motor coil, incorporate a protection circuit into the design to prevent device malfunction or breakdown caused by the current resulting from the inrush current at power ON or the negative current resulting from the back electromotive force at power OFF. IC breakdown may cause injury, smoke or ignition.

 Use a stable power supply with ICs with built-in protection functions. If the power supply is unstable, the protection function may not operate, causing IC breakdown. IC breakdown may cause injury, smoke or ignition.
- (4) Do not insert devices in the wrong orientation or incorrectly. Make sure that the positive and negative terminals of power supplies are connected properly. Otherwise, the current or power consumption may exceed the absolute maximum rating, and exceeding the rating(s) may cause the device breakdown, damage or deterioration, and may result injury by explosion or combustion. In addition, do not use any device that is applied the current with inserting in the wrong orientation or incorrectly even just one time.
- (5) Carefully select external components (such as inputs and negative feedback capacitors) and load components (such as speakers), for example, power amp and regulator.

 If there is a large amount of leakage current such as input or negative feedback condenser, the IC output DC voltage will increase. If this output voltage is connected to a speaker with low input withstand voltage, overcurrent or IC failure can cause smoke or ignition. (The over current can cause smoke or ignition from the IC itself.) In particular, please pay attention when using a Bridge Tied Load (BTL) connection type IC that inputs output DC voltage to a speaker directly.

Points to Remember on Handling of ICs

(1) Heat Radiation Design

In using an IC with large current flow such as power amp, regulator or driver, please design the device so that heat is appropriately radiated, not to exceed the specified junction temperature (Tj) at any time and condition. These ICs generate heat even during normal use. An inadequate IC heat radiation design can lead to decrease in IC life, deterioration of IC characteristics or IC breakdown. In addition, please design the device taking into considerate the effect of IC heat radiation with peripheral components.

(2) Back-EMF

When a motor rotates in the reverse direction, stops or slows down abruptly, a current flow back to the motor's power supply due to the effect of back-EMF. If the current sink capability of the power supply is small, the device's motor power supply and output pins might be exposed to conditions beyond maximum ratings. To avoid this problem, take the effect of back-EMF into consideration in system design.

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