

Operational Amplifiers/Buffers

LF 147/347 Wide Bandwidth Quad JFET Input Operational Amplifier

General Description

The Harris LF147 is a low cost, high speed quad JFET input operational amplifier with an internally trimmed input offset voltage. The device requires a low supply current and yet maintains a large gain bandwidth product and a fast slew rate. In addition, well matched high voltage JFET input devices provide very low input bias and offset currents. The LF147 is pin compatible with the standard LM348. This feature allows designers to immediately upgrade the overall performance of existing LM348 and LM324 designs.

The LF147 may be used in applications such as high speed integrators, fast D/A converters, sample-and-hold circuits and many other circuits requiring low input offset voltage, low input bias current, high input impedance, high slew rate and wide bandwidth. The device has low noise and offset voltage drift.

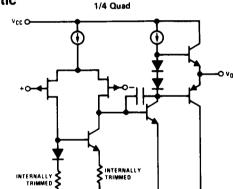
Features

■ Fast settling time to 0.01%

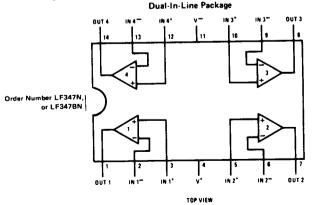
١V
Α
Ηz
Ηz
μs
ıA
Ω^{2}
2%
Hz

2 μς

Simplified Schematic



Connection Diagram



Order Number LF147J, LF347J

Absolute Maximu	m Ratings				LF347B/
	LF147	LF347B/ LF347	Power Dissipation (Note 3)	LF147 900mW	LF347 500mW
Supply Voltage Differential Input Voltage Input Voltage Range (Note 1)	±22V ±38V ±19V	±18V ±30V ±15V	T j max $ heta j AOperating TemperatureRange$	150°C 100°C/W (Note 4)	115°C 150°C/W (Note 4)
Output Short Circuit Duration (Note 2)	Continuous	Continuous	Storage Temperature Range	-65°C ≤1	T _A ≤ 150°C
			Lead Temperature (Soldering, 10 seconds)	300°C	300oC

DC Electrical Characteristics (Note 4)

SYMBOL	PARAMETER	CONDITIONS	LF147				LF347B		LF347			T
			MIN	TYP	MAX	MIN	TYP	MAX	MIN	TYP	MAX	UNITS
vos	Input Offset Voltage	R _S = 10 kΩ, T _A = 25°C		1	5		3	5		5	10	mV
	İ	Over Temperature	ł		8		l	7	1] -	13	mV
∆V _{OS} /∆T	Average TC of Input Offset Voltage	R _S = 10 kΩ		10			10		İ	10		μV/°C
los	Input Offset Current	T _j = 25°C, (Notes 5,6)		25	100		25	100	Į	25	100	ρA
		Over Temp.			25			4			4	nA
lB .	Input Bias Current	Tj = 25°C, (Notes 5,6)		50	200		50	200		50	200	рΑ
		Over Temp.		1	50		İ	8	1		8	nA
RIN	Input Resistance	T _j = 25°C		1012		1	1012			1012		Ω
AVOL	Large Signal Voltage Gain	V _S = ±15V, T _A = 25°C	50	100		50	100		25	100		V/mV
		V_{ij} = ±10V, RL = 2 k Ω		i .			l					
		Over Temperature	25			25			15	i		V/mV
٧o	Output Voltage Swing	VS = ±15V, RL = 10 kΩ	±12	±13.5		112	113.5		: 12	:13.5		v
V _{CM}	Input Common-Mode Voltage	Vs = ±15V	±11	+15		711	+15		:11	+15		v
	Range	13 2.01	-11	-12			12		211	-12		v
CMRR	Common-Mode Rejection Ratio	$R_S \le 10 \ k\Omega$	80	100		80	100		70	100		₫B
PSRR	Supply Voltage Rejection Ratio	(Note 7)	80	100		80	100		70	100		dB
1s	Supply Current			7.2	11		7.2	11		7.2	11	mA

AC Electrical Characteristics (Note 4)

SYMBOL	PARAMETER	CONDITIONS	LF147			LF347B			LF347			
			MIN	TYP	MAX	MIN	TYP	MAX	MIN	TYP	MAX	UNITS
	Amplifier to Amplifier Coupling			-120			- 120			-120	-	dB
		f = 1 Hz-20 kHz (Input Referred)					•					
SR	Slew Rate	Vg = ±15V, TA = 25°C		13			13			13		V/μs
GBW	Gain-Bandwidth Product	VS = \$15V, TA = 25 C		4			4			4		MHz
en	Equivalent Input Noise Voltage	$T_A = 25^{\circ} C$, $R_S = 100\Omega$, t = 1000 Hz		20			20			20		nV/√Hz
in	Equivalent Input Noise Current	$T_j = 25^{\circ}C$, $f = 1000 \text{ Hz}$		0.01			0.01			0.01		pA/√Hz

Note 1: For operating at elevated temperature, the device must be derated based on a thermal resistance of 125°C/W junction to ambient or 95°C/W junction to case.

Note 2: Unless otherwise specified the absolute maximum negative input voltage is equal to the negative power supply voltage.

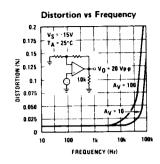
Note 3: P_D max rating cannot be exceeded.

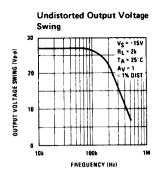
Note 4: These specifications apply for $V_S = \pm 15V$ and $0^{\circ}C \le T_A \le +70^{\circ}C$. V_{OS} , I_B and I_{OS} are measured at $V_{CM} = 0$.

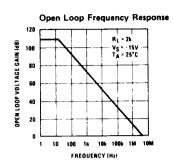
Note 5: The input bias currents are junction leakage currents which approximately double for every 10°C increase in the junction temperature, Tj. Due to limited production test time, the input bias currents measured are correlated to junction temperature. In normal operation the junction temperature rises above the ambient temperature as a result of internal power dissipation, PD. Tj = TA + Θ_{jA} PD where Θ_{jA} is the thermal resistance from junction to ambient. Use of a heat sink is recommended if input bias current is to be kept to a minimum,

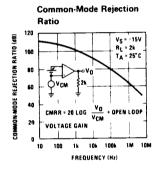
Note 6: Supply voltage rejection ratio is measured for both supply magnitudes increasing or decreasing simultaneously in accordance with common practice.

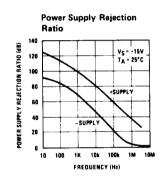
Typical Performance Characteristics (Continued)

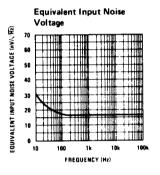


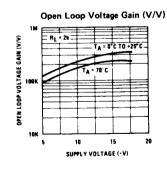


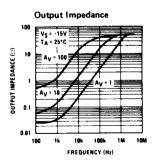


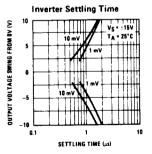


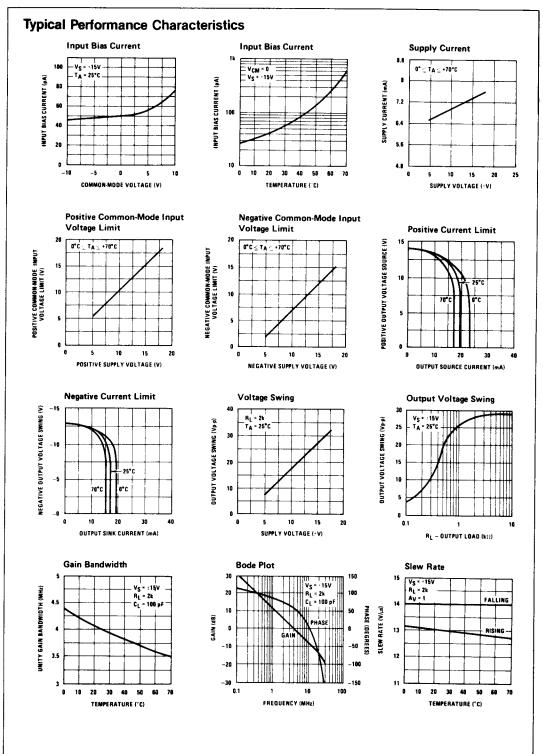




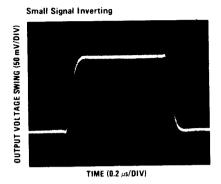




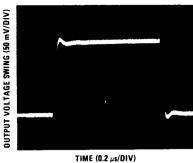




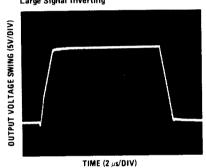
Pulse Response



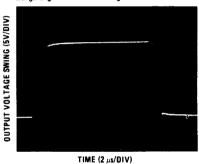
Small Signal Non-Inverting



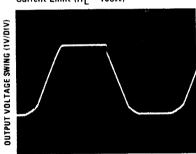
Large Signal Inverting



Large Signal Non-Inverting



Current Limit (R_L = 100 Ω)



TIME (5 µs/DIV)

Application Hints

The LF147 is an op amp with an internally trimmed input offset voltage and JFET input devices. These JFETs have large reverse breakdown voltages from gate to source and drain eliminating the need for clamps across the inputs. Therefore, large differential input voltages can easily be accommodated without a large increase in input current. The maximum differential input voltage is independent of the supply voltages.

to exceed the negative supply as this will cause large currents to flow which can result in a destroyed unit.

Exceeding the negative common-mode limit on either input will cause a reversal of the phase to the output and force the amplifier output to the corresponding high or low state. Exceeding the negative common-mode limit on both inputs will force the amplifier output to a

Application Hints (Continued)

high state. In neither case does a latch occur since raising the input back within the common-mode range again puts the input stage and thus the amplifier in a normal operating mode.

Exceeding the positive common-mode limit on a single input will not change the phase of the output; however, if both inputs exceed the limit, the output of the amplifier will be forced to a high state.

The amplifiers will operate with a common-mode input voltage equal to the positive supply; however, the gain bandwidth and slew rate may be decreased in this condition. When the negative common-mode voltage swings to within 3V of the negative supply, an increase in input offset voltage may occur.

Each amplifier is individually biased by a zener reference which allows normal circuit operation on ±4V power supplies. Supply voltages less than these may result in lower gain bandwidth and slew rate.

The LF147 will drive a $2k\,\Omega$ load resistance to $\pm 10V$ over the full temperature range if the amplifier is forced to drive heavier load currents, however, an increase in input offset voltage may occur on the negative voltage swing and finally reach an active current limit on both positive and negative swings.

Precautions should be taken to ensure that the power supply for the integrated circuit never becomes reversed in polarity or that the unit is not inadvertently installed

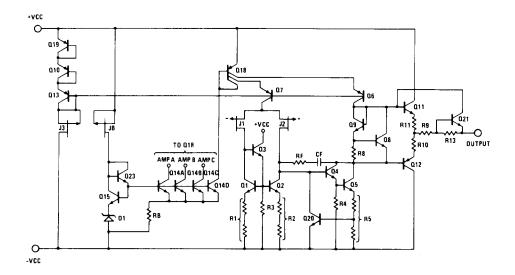
backwards in a socket as an unlimited current surge through the resulting forward diode within the IC could cause fusing of the internal conductors and result in a destroyed unit.

Because these amplifiers are JFET rather than MOSFET input op amps they do not require special handling.

As with most amplifiers, care should be taken with lead dress, component placement and supply decoupling in order to ensure stability. For example, resistors from the output to an input should be placed with the body close to the input to minimize "pick-up" and maximize the frequency of the feedback pole by minimizing the capacitance from the input to ground.

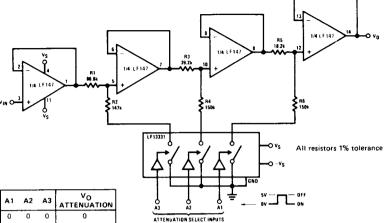
A feedback pole is created when the feedback around any amplifier is resistive. The parallel resistance and capacitance from the input of the device (usually the inverting input) to AC ground set the frequency of the pole. In many instances the frequency of this pole is much greater than the expected 3 dB frequency of the closed loop gain and consequently there is negligible effect on stability margin. However, if the feedback pole is less than approximately 6 times the expected 3 dB frequency a lead capacitor should be placed from the output to the input of the op amp. The value of the added capacitor should be such that the RC time constant of this capacitor and the resistance it parallels is greater than or equal to the original feedback pole time constant.

Detailed Schematic



Typical Applications

Digitally Selectable Precision Attenuator



- A1 A2 A3 ATTENUATION

 0 0 0 0

 0 0 1 -1 dB

 0 1 0 -2 dB

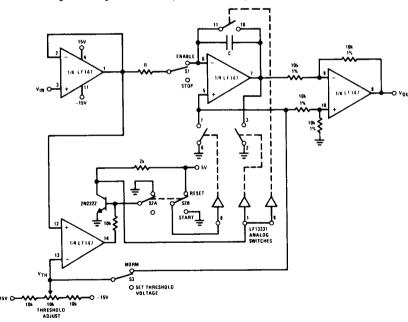
 1 0 0 -4 dB

 1 0 1 -5 dB

 1 1 0 -6 dB

 1 1 1 0 -7 dB
- · Accuracy of better than 0.4% with standard 1% value resistors
- No offset adjustment necessary
- Expandable to any number of stages
- Very high input impedance

Long Time Integrator with Reset, Hold and Starting Threshold Adjustment



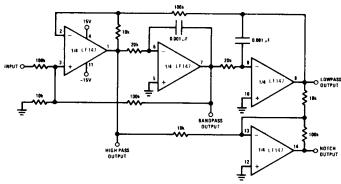
V_{OUT} starts from zero and is equal to the integral of the input voltage with respect to the threshold voltage:

$$V_{OUT} = \frac{1}{RC} \int_0^t (V_{IN} - V_{TH}) dt$$

- Output starts when $V_{1N} \ge V_{TH}$
- Switch S1 permits stopping and holding any output value
- Switch S2 resets system to zero

Typical Applications (Continued)

Universal State Variable Filter



For circuit shown: f_o = 3 kHz, f_{NOTCH} = 9.5 kHz Q = 3.4 Passband gain: Highpass - 0.1 Bandpass - 1 Lowpass - 1 Notch - 10

- $f_0 \times Q \le 200 \text{ kHz}$ 10V peak sinusoidal output swing without slew limiting to 200 kHz
- See LM348 data sheet for design equations