## Rochester Electronics Manufactured Components

Rochester branded components are manufactured using either die/wafers purchased from the original suppliers or Rochester wafers recreated from the original IP. All recreations are done with the approval of the OCM.

Parts are tested using original factory test programs or Rochester developed test solutions to guarantee product meets or exceed the OCM data sheet.

## Quality Overview

- ISO-9001
- AS9120 certification
- Qualified Manufacturers List (QML) MIL-PRF35835
- Class Q Military
- Class V Space Level
- Qualified Suppliers List of Distributors (QSLD)
- Rochester is a critical supplier to DLA and meets all industry and DLA standards.

Rochester Electronics, LLC is committed to supplying products that satisfy customer expectations for quality and are equal to those originally supplied by industry manufacturers.

The original manufacturer's datasheet accompanying this document reflects the performance and specifications of the Rochester manufactured version of this device. Rochester Electronics guarantees the performance of its semiconductor products to the original OEM specifications. 'Typical' values are for reference purposes only. Certain minimum or maximum ratings may be based on product characterization, design, simulation, or sample testing.

| Qnational semiconductor |  |
| :---: | :---: |
| LMX2330A/LMX2331A/LMX2332A |  |
| PLLatinum ${ }^{\text {TM }}$ Dual Frequency Synthesizer for RF Personal Communications |  |
|  |  |
| LMX2330A $\quad 2.5 \mathrm{GHz} / 510 \mathrm{MHz}$ | The LMX233xA are available in a TSSOP 20-pin surface mount plastic package. |
| LMX2331A $\quad 2.0 \mathrm{GHz} / 510 \mathrm{MHz}$ |  |
| LMX2332A $1.2 \mathrm{GHz} / 510 \mathrm{MHz}$ | Features |
| General Description | - 2.7 TV V 0.5 .5 V operation |
| LMX2333A family of monolitic, integrated dua | - Selectable powercown mode: $\mathrm{Icc}^{\text {c }} 1 \mathrm{HA}$ Aypical a |
| quency synthesiziess, including prescaliers, is to be used as a | ooduus prescaler: |
|  |  |
|  |  |
| The Lux233xA contains dual modulus prescalers. A 64465 | ■ Selectable charge pump TRI-STATE ${ }^{\oplus}$ mode |
|  | - Smal outine, plastic, surface mount TSSOP |
| 89 or a $16 / 1 / 7$ prescaler can be selected for the $1 F$ s synthe- | wide package |
| technique, combined with a high ¢uality reference oscillator | Applications |
| and loop fiters, provides the turing voltaes tor voltag | able Wireless Commuricaitons (PCSPCN, cordess) |
| - | diless and celluar ter |
| via |  |
| nge from 2.7 V to |  |
| very low | Other wireless communication systems |
| LMM233A-13 mA at 3 VV, LMX2331A |  |

Functional Block Diagram


TRI-STATE® is a registered trademark of National Semiconductor Corporation
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## Connection Diagram

## Thin Shrink Small Outline Package (TM)

| $V_{C C}{ }^{1}-$ | ${ }_{1} \mathrm{O}$ | 20 |
| :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{P}} 1-$ | 2 | 19 |
| $\mathrm{D}_{0} \mathrm{RF}-$ | 3 | 18 |
| GND - | 4 | 17 |
| $\mathrm{f}_{\mathrm{IN}} \mathrm{RF}$ - | 5 Top View | 16 |
| $\overline{f_{\mathrm{IN}}} R F-$ | 6 | 15 |
| GND - | 7 | 14 |
| $\mathrm{OSC}_{\text {in }}$ | 8 | 13 |
| GND - | 9 | 12 |
| $F_{0} L D-$ | 10 | 11 |

Order Number LMX2330ATM, LMX2331ATM or LMX2332ATM NS Package Number MTC20

## Pin Description

| Pin <br> No. | Pin Name | 1/0 | Description |
| :---: | :---: | :---: | :---: |
| 1 | $\mathrm{V}_{\mathrm{cC}} 1$ | - | Power supply voltage input for RF analog and RF digital circuits. Input may range from 2.7V to 5.5 V . $\mathrm{V}_{\mathrm{CC}} 1$ must equal $\mathrm{V}_{\mathrm{CC}} 2$. Bypass capacitors should be placed as close as possible to this pin and be connected directly to the ground plane. |
| 2 | $\mathrm{V}_{\mathrm{P}} 1$ | - | Power Supply for RF charge pump. Must be $\geq \mathrm{V}_{\mathrm{CC}}$. |
| 3 | DoRF | O | Internal charge pump output. For connection to a loop filter for driving the input of an external VCO. |
| 4 | GND | - | Ground for RF digital circuitry. |
| 5 | $\mathrm{f}_{\mathrm{IN}}$ RF | 1 | RF prescaler input. Small signal input from the VCO. |
| 6 | $\overline{\mathrm{f}_{\text {IN }}} \mathrm{RF}$ | 1 | RF prescaler complementary input. A bypass capacitor should be placed as close as possible to this pin and be connected directly to the ground plane. Capacitor is optional with some loss of sensitivity. |
| 7 | GND | - | Ground for RF analog circuitry. |
| 8 | $\mathrm{OSC}_{\text {in }}$ | 1 | Oscillator input. The input has a $\mathrm{V}_{\mathrm{CC}} / 2$ input threshold and can be driven from an external CMOS or TTL logic gate. |
| 9 | GND | - | Ground for IF digital, MICROWIRE ${ }^{\text {TM }}$, $\mathrm{F}_{\circ}$ LD, and oscillator circuits. |
| 10 | $F_{0}$ LD | O | Multiplexed output of the RF/IF programmable or reference dividers, RF/IF lock detect signals and Fastlock mode. CMOS output (see Programmable Modes). |
| 11 | Clock | 1 | High impedance CMOS Clock input. Data for the various counters is clocked in on the rising edge, into the 22-bit shift register. |
| 12 | Data | 1 | Binary serial data input. Data entered MSB first. The last two bits are the control bits. High impedance CMOS input. |
| 13 | LE | 1 | Load enable high impedance CMOS input. When LE goes HIGH, data stored in the shift registers is loaded into one of the 4 appropriate latches (control bit dependent(. |
| 14 | GND | - | Ground for IF analog circuitry. |
| 15 | $\overline{\mathrm{f}_{\text {IN }}} \mathrm{IF}$ | 1 | IF prescaler complementry input. A bypass capacitor should be placed as close as possible to this pin and be connected directly to the ground plane. Capacitor is optional with some loss of sensitivity. |
| 16 | $\mathrm{f}_{\text {IN }}$ IF | 1 | IF prescaler input. Small signal input from the VCO. |
| 17 | GND | - | Ground for IF digital, MICROWIRE, $\mathrm{F}_{0}$ LD, and oscillator circuits. |
| 18 | $\mathrm{D}_{0} \mathrm{IF}$ | O | IF charge pump output. For connection to a loop filter for driving the input of an external VCO. |
| 19 | $\mathrm{V}_{\mathrm{P}} 2$ | - | Power Supply for IF charge pump. Must be $\geq \mathrm{V}_{\text {cc }}$. |




## Electrical Characteristics

$V_{C C}=3.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{P}}=3.0 \mathrm{~V} ;-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<85^{\circ} \mathrm{C}$, except as specified

| Symbol | Parameter |  | Conditions | Value |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min | Typ | Max |  |
| $\mathrm{I}_{\mathrm{cc}}$ | Power Supply Current | LMX2330A RF + IF |  | $\mathrm{V}_{\mathrm{CC}}=2.7 \mathrm{~V}$ to 5.5 V |  | 13 | 16.5 | mA |
|  |  | LMX2330A RF Only |  |  | 10 | 13 |  |  |
|  |  | LMX2331A RF + IF |  |  | 12 | 15.5 |  |  |
|  |  | LMX2331A RF Only |  |  | 9 | 12 |  |  |
|  |  | LMX2332A IF + RF |  |  | 8 | 10.5 |  |  |
|  |  | LMX2332A RF Only |  |  | 5 | 7 |  |  |
|  |  | LMX233XA IF Only |  |  | 3 | 3.5 |  |  |
| $\mathrm{I}_{\text {CC-PWDN }}$ | Powerdown Current |  |  |  | 1 | 25 | $\mu \mathrm{A}$ |  |
| $\mathrm{f}_{\text {IN }} \mathrm{RF}$ | Operating Frequency | LMX2330A |  | 0.5 |  | 2.5 | GHz |  |
|  |  | LMX2331A |  | 0.2 |  | 2.0 |  |  |
|  |  | LMX2332A |  | 0.1 |  | 1.2 |  |  |
| $\mathrm{f}_{\text {IN }} \mathrm{IF}$ | Operating Frequency | LMX233XA |  | 45 |  | 510 | MHz |  |
| $\mathrm{f}_{\mathrm{OSC}}$ | Oscillator Frequency |  |  | 5 |  | 40 | MHz |  |
| f $\phi$ | Phase Detector Frequency |  |  |  |  | 10 | MHz |  |
| $\mathrm{Pf}_{\mathrm{IN}} \mathrm{RF}$ | RF Input Sensitivity |  | $\mathrm{V}_{\mathrm{CC}}=3.0 \mathrm{~V}$ | -15 |  | +4 | dBm |  |
|  |  |  | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}$ | -10 |  | +4 | dBm |  |
| $\mathrm{Pf}_{\text {IN }} \mathrm{IF}$ | IF Input Sensitivity |  | $\mathrm{V}_{\mathrm{CC}}=2.7 \mathrm{~V}$ to 5.5 V | -10 |  | +4 | dBm |  |
| $\mathrm{V}_{\text {OSC }}$ | Oscillator Sensitivity |  | $\mathrm{OSC}_{\text {in }}$ | 0.5 |  |  | $\mathrm{V}_{\mathrm{PP}}$ |  |
| $\mathrm{V}_{\mathrm{IH}}$ | High-Level Input Voltage |  | * | $0.8 \mathrm{~V}_{\mathrm{CC}}$ |  |  | V |  |
| $\mathrm{V}_{\text {IL }}$ | Low-Level Input Voltage |  | * |  |  | $0.2 \mathrm{~V}_{\mathrm{CC}}$ | V |  |
| $\xrightarrow{\mathrm{I}_{\mathrm{H}}}$ | High-Level Input Current |  | $\mathrm{V}_{\mathrm{IH}}=\mathrm{V}_{\mathrm{CC}}=5.5 \mathrm{~V}^{*}$ | -1.0 |  | 1.0 | $\mu \mathrm{A}$ |  |
| $\mathrm{I}_{\text {IL }}$ | Low-Level Input Current |  | $\mathrm{V}_{\mathrm{IL}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CC}}=5.5 \mathrm{~V}^{*}$ | -1.0 |  | 1.0 | $\mu \mathrm{A}$ |  |
| $\mathrm{I}_{\mathrm{IH}}$ | Oscillator Input Current |  | $\mathrm{V}_{\text {IH }}=\mathrm{V}_{\mathrm{CC}}=5.5 \mathrm{~V}$ |  |  | 100 | $\mu \mathrm{A}$ |  |
| $\mathrm{I}_{\text {IL }}$ | Oscillator Input Current |  | $\mathrm{V}_{\mathrm{IL}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CC}}=5.5 \mathrm{~V}$ | -100 |  |  | $\mu \mathrm{A}$ |  |
| $\mathrm{V}_{\mathrm{OH}}$ | High-Level Output Voltage |  | $\mathrm{I}_{\mathrm{OH}}=-500 \mu \mathrm{~A}$ | $\mathrm{V}_{\mathrm{CC}}-0.4$ |  |  | V |  |
| $\mathrm{V}_{\mathrm{OL}}$ | Low-Level Output Voltage |  | $\mathrm{I}_{\mathrm{OL}}=500 \mu \mathrm{~A}$ |  |  | 0.4 | V |  |
| $\mathrm{t}_{\mathrm{CS}}$ | Data to Clock Set Up Time |  | See Data Input Timing | 50 |  |  | ns |  |
| $\mathrm{t}_{\mathrm{CH}}$ | Data to Clock Hold Time |  | See Data Input Timing | 10 |  |  | ns |  |
| $\mathrm{t}_{\text {CWH }}$ | Clock Pulse Width High |  | See Data Input Timing | 50 |  |  | ns |  |
| $\mathrm{t}_{\mathrm{CWL}}$ | Clock Pulse Width Low |  | See Data Input Timing | 50 |  |  | ns |  |
| $\mathrm{t}_{\text {ES }}$ | Clock to Load Enable Set Up Time |  | See Data Input Timing | 50 |  |  | ns |  |
| $\mathrm{t}_{\text {EW }}$ | Load Enable Pulse Width |  | See Data Input Timing | 50 |  |  | ns |  |

*Clock, Data and LE. Does not include $\mathrm{f}_{\mathrm{IN}}$ RF, $\mathrm{f}_{\mathrm{IN}}$ IF and $\mathrm{OSC}_{\mathrm{IN}_{\mathrm{N}}}$
Note 1: Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Recommended Operating Conditions indicate conditions for which the device is intended to be functional, but do not guarantee specific performance limits. For guaranteed specifications and test conditions, see the Electrical Characteristics. The guaranteed specifications apply only for the test conditions listed.
Note 2: This device is a high performance RF integrated circuit with an ESD rating $<2 \mathrm{keV}$ and is ESD sensitive. Handling and assembly of this device should only be done at ESD protected workstations.

## Charge Pump Characteristics

$\mathrm{V}_{\mathrm{CC}}=3.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{P}}=3.0 \mathrm{~V} ;-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<85^{\circ} \mathrm{C}$, except as specified

| Symbol | Parameter | Conditions | Value |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min | Typ | Max |  |
| $\mathrm{I}_{\mathrm{D}_{0} \text {-SOURCE }}$ | Charge Pump Output Current | $\mathrm{V}_{\mathrm{D}_{0}}=\mathrm{V}_{\mathrm{P}} / 2, \mathrm{I}_{\mathrm{CP}_{0}}=\mathrm{HIGH}^{* *}$ |  | -4.5 |  | mA |
| $\mathrm{I}_{\mathrm{D}_{0} \text {-SINK }}$ |  | $\mathrm{V}_{\mathrm{D}_{0}}=\mathrm{V}_{\mathrm{P}} / 2, \mathrm{I}_{\mathrm{CP}_{0}}=\mathrm{HIGH}^{* *}$ |  | 4.5 |  | mA |
| $\mathrm{I}_{\mathrm{D}_{0} \text {-SOURCE }}$ |  | $\mathrm{V}_{\mathrm{D}_{0}}=\mathrm{V}_{\mathrm{P}} / 2, \mathrm{I}_{\mathrm{CP}_{0}}=\mathrm{LOW}^{* *}$ |  | -1.125 |  | mA |
| $\mathrm{I}_{\mathrm{D}_{0} \text {-SINK }}$ |  | $\mathrm{V}_{\mathrm{D}_{0}}=\mathrm{V}_{\mathrm{P}} / 2, \mathrm{I}_{\mathrm{CP}_{0}}=\mathrm{LOW}^{* *}$ |  | 1.125 |  | mA |
| $\mathrm{I}_{\mathrm{D}_{0} \text {-TRI }}$ | Charge Pump TRI-STATE Current | $\begin{aligned} & 0.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{D}_{0}} \leq \mathrm{V}_{\mathrm{P}}-0.5 \mathrm{~V} \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<85^{\circ} \mathrm{C} \end{aligned}$ | -2.5 |  | 2.5 | nA |
| $\begin{aligned} & \mathrm{I}_{\mathrm{D}_{0} \text { SINK }} \mathrm{VS} \\ & \mathrm{I}_{\mathrm{D}_{0} \text {-SOURCE }} \end{aligned}$ | CP Sink vs Source Mismatch (Note 4) | $\begin{aligned} & \mathrm{V}_{\mathrm{D}_{0}}=\mathrm{V}_{\mathrm{P}} / 2 \\ & \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C} \end{aligned}$ |  | 3 | 10 | \% |
| $\mathrm{I}_{\mathrm{D}_{0}} \mathrm{vs} \mathrm{V}_{\mathrm{D}_{0}}$ | CP Current vs Voltage (Note 3) | $\begin{aligned} & 0.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{D}_{0}} \leq \mathrm{V}_{\mathrm{P}}-0.5 \mathrm{~V} \\ & \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C} \end{aligned}$ |  | 10 | 15 | \% |
| $\mathrm{I}_{\mathrm{D}_{0}}$ vs $\mathrm{T}_{\mathrm{A}}$ | CP Current vs Temperature (Note 5) | $\begin{aligned} & \mathrm{V}_{\mathrm{D}_{o}}=\mathrm{V}_{\mathrm{P}} / 2 \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<85^{\circ} \mathrm{C} \end{aligned}$ |  | 10 |  | \% |

** See PROGRAMMABLE MODES for $\mathrm{I}_{\mathrm{CPo}}$ description.
Note 3: See charge pump current specification definitions below.
Note 4: See charge pump current specification definitions below.
Note 5: See charge pump current specification definitions below.

## Charge Pump Current Specification Definitions


$I 1=C P$ sink current at $\mathrm{V}_{\mathrm{Do}}=\mathrm{V}_{\mathrm{P}}-\Delta \mathrm{V}$
$12=C P$ sink current at $V_{D o}=V_{P} / 2$
$13=C P$ sink current at $V_{\text {Do }}=\Delta V$
$4=C P$ source current at $V_{D o}=V_{P}-\Delta V$
$15=C P$ source current at $V_{D o}=V_{P} / 2$
I6 $=\mathrm{CP}$ source current at $\mathrm{V}_{\mathrm{D}_{0}}=\Delta \mathrm{V}$
$\Delta \mathrm{V}=$ Voltage offset from positive and negative rails. Dependent on VCO tuning range relative to $\mathrm{V}_{\mathrm{CC}}$ and ground. Typical values are between 0.5 V and 1.0 V .
3. $I_{\text {Do }}$ vs $V_{D o}=$ Charge Pump Output Current magnitude variation vs Voltage $=$
$[1 / 2 *\{|11|-||3|\}] /[1 / 2 *\{|11|+||3|\}] * 100 \%$ and $[1 / 2 *\{| | 4|-||6|\}] /[1 / 2 *\{| | 4|+|16|\}] * 100 \%$
4. $I_{\text {Do-sink }}$ vs $I_{\text {Do-source }}=$ Charge Pump Output Current Sink vs Source Mismatch $=$
[||2| - |15|]/[1⁄2 * \{||2| + |15|\}] * 100\%
5. $\mathrm{I}_{\mathrm{Do}}$ vs $\mathrm{T}_{\mathrm{A}}=$ Charge Pump Output Current magnitude variation vs Temperature $=$
$\left[\left|\mid 2\right.\right.$ @templ-||2 @ $\left.\left.25^{\circ} \mathrm{C}\right|\right] /\left|12 @ 25^{\circ} \mathrm{C}\right| * 100 \%$ and $\left[\left|\mid 15\right.\right.$ @temp| - | 15 @ $\left.\left.25^{\circ} \mathrm{C}\right|\right] /\left|\left|5 @ 25^{\circ} \mathrm{C}\right| * 100 \%\right.$

## RF Sensitivity Test Block Diagram



Note: $N=10,000 \mathrm{R}=50 \mathrm{P}=64$
Note: Sensitivity limit is reached when the error of the divided RF output, $F_{0} L D$, is $\geq 1 \mathrm{~Hz}$.

## Typical Performance Characteristics



$\mathrm{I}_{\mathrm{cc}}$ vs $\mathrm{V}_{\mathrm{cc}}$
LMX2332A



Charge Pump Current vs $D_{o}$ Voltage
$I_{C P}=H I G H$


Charge Pump Current vs $\mathrm{D}_{\mathrm{o}}$ Voltage $I_{C P}=$ LOW


## Typical Performance Characteristics (Continued)

Charge Pump Current Variation
(See Note 3 under Charge Pump Current Specification Definitions)


RF Input Impedance
$\mathrm{V}_{\mathrm{cc}}=2.7 \mathrm{~V}$ to $5.5 \mathrm{~V}, \mathrm{f}_{\mathrm{IN}}=50 \mathrm{MHz}$ to 3 GHz


Marker $1=1 \mathrm{GHz}$, Real $=101$, Imag. $=-144$
Marker $2=2 \mathrm{GHz}$, Real $=37$, Imag. $=-54$
Marker $3=3 \mathrm{GHz}$, Real $=22$, Imag. $=-2$
Marker $4=500 \mathrm{MHz}$, Real $=209$, Imag. $=-232$

Sink vs Source Mismatch
(See Note 4 under Charge Pump Current Specification Definitions)


IF Input Impedance
$\mathrm{V}_{\mathrm{Cc}}=2.7 \mathrm{~V}$ to $5.5 \mathrm{~V}, \mathrm{f}_{\mathrm{IN}}=10 \mathrm{MHz}$ to 1000 MHz


Marker $1=100 \mathrm{MHz}$, Real $=589$, Imag. $=-209$
Marker $2=200 \mathrm{MHz}$, Real $=440$, Imag. $=-286$
Marker $3=300 \mathrm{MHz}$, Real $=326$, Imag. $=-287$
Marker $4=500 \mathrm{MHz}$, Real $=202$, Imag. $=-234$

## Typical Performance Characteristics (Continued)



LMX2331A RF Sensitivity vs Frequency


LMX2332A RF Sensitivity vs Frequency


IF Input Sensitivity vs Frequency


## Oscillator Input Sensitivity vs Frequency



## Functional Description

The simplified block diagram below shows the 22-bit data register, two 15 -bit R Counters and the 15 - and 18 -bit N Counters (in termediate latches are not shown). The data stream is clocked (on the rising edge of Clock) into the DATA register, MSB first. The data stored in the shift register is loaded into one of 4 appropriate latches on the rising edge of LE. The last two bits are the Control Bits. The DATA is transferred into the counters as follows:

| Control Bits |  | DATA Location |
| :---: | :---: | :---: |
| C1 | C2 |  |
| 0 | 0 | IF R Counter |
| 0 | 1 | RF R Counter |
| 1 | 0 | IF N Counter |
| 1 | 1 | RF N Counter |



PROGRAMMABLE REFERENCE DIVIDERS (IF AND RF R COUNTERS)
If the Control Bits are 00 or 01 ( 00 for IF and 01 for RF) data is transferred from the 22 -bit shift register into a latch which sets the 15 -bit R Counter. Serial data format is shown below.


15-BIT PROGRAMMABLE REFERENCE DIVIDER RATIO (R COUNTER)

| Divide | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ | $\mathbf{R}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ratio | $\mathbf{1 5}$ | $\mathbf{1 4}$ | $\mathbf{1 3}$ | $\mathbf{1 2}$ | $\mathbf{1 1}$ | $\mathbf{1 0}$ | $\mathbf{9}$ | $\mathbf{8}$ | $\mathbf{7}$ | $\mathbf{6}$ | $\mathbf{5}$ | $\mathbf{4}$ | $\mathbf{3}$ | $\mathbf{2}$ | $\mathbf{1}$ |
| 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 |
| $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ |
| 32767 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |

Notes:
Divide ratios less than 3 are prohibited.
Divide ratio: 3 to 32767
R1 to R15: These bits select the divide ratio of the programmable reference divider
Data is shifted in MSB first.

## Functional Description (Continued)

## PROGRAMMABLE DIVIDER (N COUNTER)

The N counter consists of the 7 -bit swallow counter ( A counter) and the 11-bit programmable counter ( B counter). If the Control Bits are 10 or 11 ( 10 for IF counter and 11 for RF counter) data is transferred from the 22-bit shift register into a 4-bit or 7-bit latch (which sets the Swallow (A) Counter) and an 11-bit latch (which sets the 11-bit programmable (B) Counter), MSB first. Serial data format is shown below. For the IF N counter bits 5, 6, and 7 are don't care bits. The RF N counter does not have don't care bits.


## 7-BIT SWALLOW COUNTER DIVIDE RATIO (A COUNTER)

RF

| Divide <br> Ratio <br> A | $\mathbf{N}$ | $\mathbf{7}$ | $\mathbf{N}$ | $\mathbf{N}$ | $\mathbf{5}$ | $\mathbf{N}$ | $\mathbf{4}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{N}$ | $\mathbf{N}$ | $\mathbf{2}$ | $\mathbf{N}$ |  |  |  |  |
| $\mathbf{1}$ |  |  |  |  |  |  |  |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| $\cdot$ | $\bullet$ | $\cdot$ | $\cdot$ | $\cdot$ | $\cdot$ | $\cdot$ | $\bullet$ |
| 127 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |

Note: Divide ratio: 0 to 127
$B \geq A$

IF

| Divide <br> Ratio <br> A | $\mathbf{N}$ | $\mathbf{7}$ | $\mathbf{N}$ | $\mathbf{N}$ | $\mathbf{N}$ | $\mathbf{N}$ | $\mathbf{N}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{5}$ | $\mathbf{4}$ | $\mathbf{3}$ | $\mathbf{2}$ | $\mathbf{1}$ |  |  |  |
| 0 | X | X | X | 0 | 0 | 0 | 0 |
| 1 | X | X | X | 0 | 0 | 0 | 1 |
| $\cdot$ | $\cdot$ | $\cdot$ | $\cdot$ | $\cdot$ | $\cdot$ | $\cdot$ | $\bullet$ |
| 15 | X | X | X | 1 | 1 | 1 | 1 |

$\mathrm{X}=$ DON'T CARE condition

11-BIT PROGRAMMABLE COUNTER DIVIDE RATIO (B COUNTER)
$\left.\begin{array}{|c|c|c|c|c|c|c|c|c|c|c|c|}\hline \begin{array}{c}\text { Divide } \\ \text { Ratio } \\ \mathbf{B}\end{array} & \begin{array}{c}\mathbf{N} \\ \mathbf{1 8}\end{array} & \begin{array}{c}\mathbf{N} \\ \mathbf{1 7}\end{array} & \begin{array}{c}\mathbf{N} \\ \mathbf{1 6}\end{array} & \begin{array}{c}\mathbf{N} \\ \mathbf{1 5}\end{array} & \begin{array}{c}\mathbf{N} \\ \mathbf{1 4}\end{array} & \begin{array}{c}\mathbf{N} \\ \mathbf{1 3}\end{array} & \begin{array}{c}\mathbf{N} \\ \mathbf{1 2}\end{array} & \begin{array}{c}\mathbf{N} \\ \mathbf{1 1}\end{array} & \begin{array}{c}\mathbf{N} \\ \mathbf{1 0}\end{array} & \begin{array}{c}\mathbf{N} \\ \mathbf{9}\end{array} & \mathbf{N} \\ \mathbf{8}\end{array}\right]$

Note: Divide ratio: 3 to 2047 (Divide ratios less than 3 are prohibited)
$B \geq A$

## PULSE SWALLOW FUNCTION

$f_{\mathrm{Vco}}=[(P \times B)+A] \times f_{o s c} / R$
$\mathrm{f}_{\mathrm{vco}}$ : Output frequency of external voltage controlled oscillator (VCO)
B: Preset divide ratio of binary 11-bit programmable counter (3 to 2047)
A: Preset divide ratio of binary 7 -bit swallow counter

$$
(0 \leq \mathrm{A} \leq 127\{\mathrm{RF}\}, 0 \leq \mathrm{A} \leq 15\{\mathrm{IF}\}, \mathrm{A} \leq \mathrm{B})
$$

$\mathrm{f}_{\text {Osc }}$ : Output frequency of the external reference frequency oscillator
R: Preset divide ratio of binary 15-bit programmable reference counter (3 to 32767)
P: Preset modulus of dual modulus prescaler (for IF ; P = 8 or 16;

$$
\text { for RF ; LMX2330A: } P=32 \text { or } 64 \quad \text { LMX2331A/32A: } P=64 \text { or 128) }
$$

## PROGRAMMABLE MODES

Several modes of operation can be programmed with bits R16-R20 including the phase detector polarity, charge pump TRI-STATE and the output of the FoLD pin. The prescaler and powerdown modes are selected with bits N19 and N20. The programmable modes are shown in Table 1. Truth table for the programmable modes and FoLD output are shown in Table 2 and Table 3.

Functional Description (Continued)
TABLE 1. Programmable Modes

| C1 | C2 | R16 | R17 | R18 | R19 | R20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | IF Phase <br> Detector Polarity | IF I $\mathrm{CP}_{\circ}$ | IF $\mathrm{D}_{\circ}$ <br> TRI-STATE | IF LD | IF $\mathrm{F}_{\circ}$ |
| 0 | 1 | RF Phase <br> Detector Polarity | RF I $\mathrm{ICP}_{\circ}$ | RF $\mathrm{D}_{\circ}$ <br> TRI-STATE | RF LD | RF F $\mathrm{F}_{\circ}$ |


| C1 | C2 | N19 | N20 |
| :---: | :---: | :---: | :---: |
| 1 | 0 | IF Prescaler | Pwdn IF |
| 1 | 1 | RF Prescaler | Pwdn RF |

TABLE 2. Mode Select Truth Table

|  | Phase Detector Polarity | D$_{\mathbf{o}}$ TRI-STATE | $\mathbf{I}_{\mathbf{C P}_{\mathbf{o}}}$ <br> $($ Note 6) | IF <br> Prescaler | 2330A RF <br> Prescaler | 2331A/32A RF <br> Prescaler | Pwdn <br> (Note 7) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | Negative | Normal <br> Operation | LOW | $8 / 9$ | $32 / 33$ | $64 / 65$ | Pwrd <br> Up |
| 1 | Positive | TRI-STATE | HIGH | $16 / 17$ | $64 / 65$ | $128 / 129$ | Pwrd <br> Dn |

Note 6: The $\mathrm{I}_{\mathrm{CPo}}$ LOW current state $=1 / 4 \times \mathrm{I}_{\mathrm{CPo}}$ HIGH current.
Note 7: Activation of the IF PLL or RF PLL powerdown modes result in the disabling of the respective $N$ counter divider and debiasing of its respective $f_{\mathrm{IN}}$ inputs (to a high impedance state). The powerdown function is gated by the charge pump to prevent unwanted frequency jumps. Once the powerdown program mode is oaded, the part will go into powerdown mode when the charge pump reaches a TRI-STATE condition. The R counter functionality does not become disabled until both IF and RF powerdown bits are activated. The MICROWIRE control register remains active and capable of loading and latching data during all of the powerdown modes.

TABLE 3. The FoLD (Pin 10) Output Truth Table

| RF R[19] <br> (RF LD) | IF R[19] <br> (IF LD) | RF R[20] <br> (RF F $\mathbf{o}_{\mathbf{o}}$ ) | IF R[20] <br> (IF F $\mathbf{o}_{\mathbf{o}}$ | Fo Output State $^{\prime}$ |
| :---: | :---: | :---: | :---: | :--- |
| 0 | 0 | 0 | 0 | Disabled (Note 8) |
| 0 | 1 | 0 | 0 | IF Lock Detect (Note 9) |
| 1 | 0 | 0 | 0 | RF Lock Detect (Note 9) |
| 1 | 1 | 0 | 0 | RF/IF Lock Detect (Note 9) |
| $X$ | 0 | 0 | 1 | IF Reference Divider Output |
| $X$ | 0 | 1 | 0 | RF Reference Divider Output |
| $X$ | 1 | 0 | 1 | IF Programmable Divider Output |
| $X$ | 1 | 1 | 0 | RF Programmable Divider Output |
| 0 | 0 | 1 | 1 | Fastlock (Note 10) |
| 0 | 1 | 1 | 1 | For Internal Use Only |
| 1 | 0 | 1 | 1 | For Internal Use Only |
| 1 | 1 | 1 | Counter Reset (Note 11) |  |

$X=$ don't care condition
Note 8: When the $F_{0}$ LD output is disabled, it is actively pulled to a low logic state.
Note 9: Lock detect output provided to indicate when the VCO frequency is in "lock." When the loop is locked and a lock detect mode is selected, the pins output is HIGH, with narrow pulses LOW. In the RF/F lock detect mode a locked condition is indicated when RF and IF are both locked.
Note 10: The Fastlock mode utilizes the $\mathrm{F}_{0}$ LD output pin to switch a second loop filter damping resistor to ground during fastlock operation. Activation of Fastlock occurs whenever the RF loop's lcpo magnitude bit \#17 is selected HIGH (while the \#19 and \#20 mode bits are set for Fastlock).
Note 11: The Counter Reset mode bits R19 and R20 when activated reset all counters. Upon removal of the Reset bits then N counter resumes counting in "close" alignment with the R counter. (The maximum error is one prescaler cycle.) If the Reset bits are activated the R counter is also forced to Reset, allowing smooth acquisition upon powering up.

Functional Description (Continued)

## PHASE DETECTOR POLARITY

Depending upon VCO characteristics, R16 bit should be set accordingly: (see figure right)
When VCO characteristics are positive like (1), R16 should be set HIGH;
When VCO characteristics are negative like (2), R16 should be set LOW.


## SERIAL DATA INPUT TIMING



Notes: Parenthesis data indicates programmable reference divider data.
Data shifted into register on clock rising edge.
Data is shifted in MSB first.
Test Conditions: The Serial Data Input Timing is tested using a symmetrical waveform around $\mathrm{V}_{\mathrm{CC}} / 2$. The test waveform has an edge rate of $0.6 \mathrm{~V} / \mathrm{ns}$ with amplitudes of $2.2 \mathrm{~V} @ \mathrm{~V}_{\mathrm{CC}}=2.7 \mathrm{~V}$ and $2.6 \mathrm{~V} @ \mathrm{~V}_{\mathrm{CC}}=5.5 \mathrm{~V}$.
PHASE COMPARATOR AND INTERNAL CHARGE PUMP CHARACTERISTICS


Notes: Phase difference detection range: $-2 \pi$ to $+2 \pi$
The minimum width pump up and pump down current pulses occur at the $D_{0}$ pin when the loop is locked. R16 $=$ HIGH

## Typical Application Example



Operational Notes:

* VCO is assumed AC coupled
** $\quad \mathrm{R}_{\mathrm{IN}}$ increases impedance so that VCO output power is provided to the load rather than the PLL. Typical values are $10 \Omega$ to $200 \Omega$ depending on the VCO power level. $f_{I N}$ RF impedance ranges from $40 \Omega$ to $100 \Omega$. $\mathrm{f}_{\mathrm{IN}}$ IF impedances are higher.
*** $50 \Omega$ termination is often used on test boards to allow use of external reference oscillator. For most typical products a CMOS clock is used and no terminating resistor is required. OSC $_{\text {in }}$ may be AC or DC coupled. AC coupling is recommended because the input circuit provides its own bias. (See Figure below)
**** Adding RC filters to the $\mathrm{V}_{\mathrm{Cc}}$ line is recommended to reduce loop-to-loop noise coupling


Proper use of grounds and bypass capacitors is essential to achieve a high level of performance. Crosstalk between pins can be reduced by careful board layout.
This is an electrostatic sensitive device. It should be handled only at static free work stations.

## Application Information

A block diagram of the basic phase locked loop is shown in Figure 1.


FIGURE 1. Basic Charge Pump Phase Locked Loop

## OOP GAIN EQUATIONS

A linear control system model of the phase feedback for a PLL in the locked state is shown in Figure 2. The open loop gain is the product of the phase comparator gain ( $K \phi$ ), the VCO gain ( $\mathrm{K}_{\mathrm{vco}} / \mathrm{s}$ ), and the loop filter gain $\mathrm{Z}(\mathrm{s})$ divided by the gain of the feedback counter modulus ( N ). The passive loop filter configuration used is displayed in Figure 3, while the complex impedance of the filter is given in Equation (2).


FIGURE 2. PLL Linear Model


FIGURE 3. Passive Loop Filter

$$
\begin{gather*}
\text { Open loop gain }=H(s) G(s)=\frac{\Theta_{i}}{\Theta_{e}}=\frac{K_{\phi} Z(s) K_{V C O}}{N s}  \tag{1}\\
Z(s)=\frac{s(C 2 \bullet R 2)+1}{s^{2}(C 1 \bullet C 2 \bullet R 2)+s C 1+s C 2} \tag{2}
\end{gather*}
$$

The time constants which determine the pole and zero frequencies of the filter transfer function can be defined as

$$
\begin{equation*}
T 1=R 2 \cdot \frac{C 1 \bullet C 2}{C 1+C 2} \tag{3}
\end{equation*}
$$

and

$$
\begin{equation*}
\mathrm{T} 2=\mathrm{R} 2 \cdot \mathrm{C} 2 \tag{4}
\end{equation*}
$$

The 3rd order PLL Open Loop Gain can be calculated in terms of frequency, $\omega$, the filter time constants T1 and T2, and the design constants $\mathrm{K}_{\phi}, \mathrm{K}_{\mathrm{vco}}$, and N .

$$
\begin{equation*}
\left.G(s) \bullet H(s)\right|_{s=j \bullet \omega}=\frac{-K_{\phi} \bullet K_{V C O}(1+j \omega \bullet T 2)}{\omega^{2} C 1 \bullet N(1+J \omega \bullet T 1)} \bullet \frac{T 1}{T 2} \tag{5}
\end{equation*}
$$

From Equation (3) we can see that the phase term will be dependent on the single pole and zero such that the phase margin is determined in Equation (6).

$$
\begin{equation*}
\phi(\omega)=\tan ^{-1}(\omega \cdot \mathrm{~T} 2)-\tan ^{-1}(\omega \cdot \mathrm{~T} 1)+180^{\circ} \tag{6}
\end{equation*}
$$

A plot of the magnitude and phase of $\mathrm{G}(\mathrm{s}) \mathrm{H}(\mathrm{s})$ for a stable loop, is shown in Figure 4 with a solid trace. The parameter $\phi_{\mathrm{p}}$ shows the amount of phase margin that exists at the point the gain drops below zero (the cutoff frequency wp of the loop). In a critically damped system, the amount of phase margin would be approximately 45 degrees.
If we were now to redefine the cut off frequency, wp', as double the frequency which gave us our original loop bandwidth, wp, the loop response time would be approximately halved. Because the filter attenuation at the comparison frequency also diminishes, the spurs would have increased by approximately 6 dB . In the proposed Fastlock scheme, the higher spur levels and wider loop filter conditions would exist only during the initial lock-on phase-just long enough to reap the benefits of locking faster. The objective would be to open up the loop bandwidth but not introduce any additional complications or compromises related to our original design criteria. We would ideally like to momentarily shift the curve of Figure 4 over to a different cutoff frequency, illustrated by the dotted line, without affecting the relative open loop gain and phase relationships. To maintain the same gain/phase relationship at twice the original cutoff frequency, other terms in the gain and phase Equations (5), (6) will have to compensate by the corresponding " $1 / w$ " or " $1 / w^{2}$ " factor. Examination of Equations (3), (4), (6) indicates the damping resistor variable R2 could be chosen to compensate the " $w$ "' terms for the phase margin. This implies that another resistor of equal value to R2 will need to be switched in parallel with R2 during the initial lock period. We must also ensure that the magnitude of the open loop gain, $\mathrm{H}(\mathrm{s}) \mathrm{G}(\mathrm{s})$ is equal to zero at wp' = $2 w p . \mathrm{K}_{\mathrm{vco}}, \mathrm{K} \phi, \mathrm{N}$, or the net product of these terms can be changed by a factor of 4 , to counteract the $\mathrm{w}^{2}$ term present in the denominator of Equations (3), (4). The K $\phi$ term was chosen to complete the transformation because it can readily be switch between 1 X and 4 X values. This is accomplished by increasing the charge pump output current from 1 mA in the standard mode to 4 mA in Fastlock.

## Application Information (Continued)



## FIGURE 4. Open Loop Response Bode Plot

## FASTLOCK CIRCUIT IMPLEMENTATION

A diagram of the Fastlock scheme as implemented in Na tional Semiconductors LMX233xA PLL is shown in Figure 5. When a new frequency is loaded, and the RF Icp. bit is set high the charge pump circuit receives an input to deliver 4 times the normal current per unit phase error while an open drain NMOS on chip device switches in a second R2 resistor element to ground. The user calculates the loop filter component values for the normal steady state considerations. The device configuration ensures that as long as a second iden-
tical damping resistor is wired in appropriately, the loop will lock faster without any additional stability considerations to account for. Once locked on the correct frequency, the user can return the PLL to standard low noise operation by sending a MICROWIRE instruction with the RF Icpo bit set low. This transition does not affect the charge on the loop filter capacitors and is enacted synchronous with the charge pump output. This creates a nearly seamless change between Fastlock and standard mode.


FIGURE 5. Fastlock PLL Architecture
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