

THOMSON SEMICONDUCTORS

LM124
LM224
LM324, A
LM2902

LOW POWER QUAD OPERATIONAL AMPLIFIERS

These circuits consist of four independent, high gain, internally frequency compensated operational amplifiers which were designed specifically for automotive and industrial control systems. They operate from a single power supply over a wide range of voltages. Operation from split power supplies is also possible and the low power supply current drain is independent of the magnitude of the power supply voltage.

- Large voltage gain : 100 dB.
- Very low supply current drain : 800 μ A.
- Low input bias current : 45 nA.
- Low input offset voltage : 2 mV.
- Low input offset current : 5 nA.

Wide power supply range :

- Single supply : +3 V to +30 V.
- Dual supplies for LM124 : ± 1.5 V to ± 15 V.
- Single supply for LM2902 : +3 V to +26 V.

ORDERING INFORMATION

Hi-Rel versions available - See chapter 14

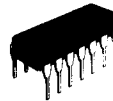
PART NUMBER	TEMPERATURE RANGE	PACKAGE			
		DP	DG	GC	FP
LM124	-55°C to +125°C		•	•	
LM224	-25°C to +85°C	•	•		
LM324, A	0°C to +70°C	•	•		•
LM2902	-40°C to +85°C	•			•

Examples : LM124DG, LM124GC, LM224DP

LOW POWER QUAD OPERATIONAL AMPLIFIERS

CASES

CB-2



DP SUFFIX
PLASTIC PACKAGE
DG SUFFIX
CERDIP PACKAGE

CB-511



FP SUFFIX
PLASTIC
MICROPACKAGE

CB-705

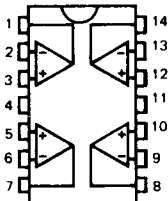


GC SUFFIX
TRICOP (LCC)

PIN ASSIGNMENTS

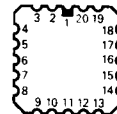
(Top views)

CB-2
CB-511



- | | |
|---------------------------|----------------------------|
| 1 - Output 1 | 8 - Output 3 |
| 2 - Inverting input 1 | 9 - Inverting input 3 |
| 3 - Non-inverting input 1 | 10 - Non-inverting input 3 |
| 4 - V_{CC} | 11 - V_{CC} |
| 5 - Non-inverting input 2 | 12 - Non-inverting input 4 |
| 6 - Inverting input 2 | 13 - Inverting input 4 |
| 7 - Output 2 | 14 - Output 4 |

CB-705



- | | |
|---------------------------|----------------------------|
| 1 - NC | 11 - NC |
| 2 - Output 1 | 12 - Output 3 |
| 3 - Inverting input 1 | 13 - Inverting input 3 |
| 4 - Non-inverting input 1 | 14 - Non-inverting input 3 |
| 5 - NC | 15 - NC |
| 6 - V_{CC} | 16 - V_{CC} |
| 7 - NC | 17 - NC |
| 8 - Non-inverting input 2 | 18 - Non-inverting input 4 |
| 9 - Inverting input 2 | 19 - Inverting input 4 |
| 10 - Output 2 | 20 - Output 4 |

THOMSON SEMICONDUCTORS

Sales headquarters
45, av. de l'Europe - 78140 VELIZY - FRANCE
Tel. : (31) 946 97 19 / Telex : 204780 F

THOMSON
SEMICONDUCTORS

MAXIMUM RATINGS

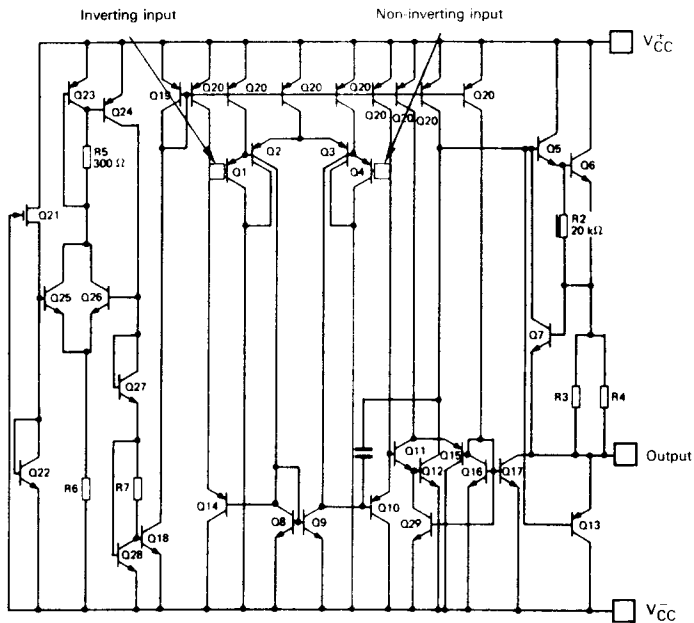
Rating	Symbol	LM124	LM224	LM324,A	LM2902	Unit
Supply voltage	V_{CC}	± 16 or 32	± 16 or 32	± 16 or 32	± 13 or 26	V
Differential input voltage	V_{ID}	32	32	32	26	V
Input voltage (Note 7)	V_I	-0.3 to +32	-0.3 to +32	-0.3 to +32	-0.3 to +26	V
Output short circuit duration ($V_{CC} = \pm 15$ V, $T_{amb} = +25^\circ\text{C}$)	—	Infinite for all amplifiers				—
Power dissipation (Note 1) LM124GC LM324FP, AFP/LM2902FP	P_{tot}	500 665	500	500 400	500 400	mW
Operating free-air temperature range	T_{oper}	-55 to +125	-25 to +85	0 to +70	-40 to +85	$^\circ\text{C}$
Storage temperature range	T_{stg}	65 to +150	65 to +150	-65 to +150	-65 to +150	$^\circ\text{C}$

Input current for $V_I \leq -0.3, V_{OL} : 50$ mA

See notes page 4

Devices bonded on a 6 cm × 3 cm × 0.15 cm glass epoxy substrate with 30 mm² of 35 μm thick copper.

SCHEMATIC DIAGRAM



CASE	Inverting inputs	Non-inverting inputs	V_{CC}	V_{CC}	Outputs	N.C.
CB-2/CB-511	2, 6, 9, 13	3, 5, 10, 12	11	4	1, 7, 8, 14	
CB-705	3, 9, 13, 19	4, 8, 14, 18	16	6	1, 2, 12, 20	*

* CB-705 : Other pins are not connected.

ELECTRICAL CHARACTERISTICS

$V_{CC}^+ = +5\text{ V}, V_{CC}^- = \text{GND}$

LM124 : $-55^\circ\text{C} \leq T_{\text{amb}} \leq +125^\circ\text{C}$

LM224 : $-25^\circ\text{C} \leq T_{\text{amb}} \leq +85^\circ\text{C}$

LM324, A : $0^\circ\text{C} \leq T_{\text{amb}} \leq +70^\circ\text{C}$

LM2902 : $-40^\circ\text{C} \leq T_{\text{amb}} \leq +85^\circ\text{C}$

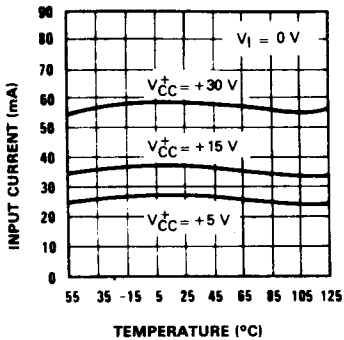
(Unless otherwise specified)

Characteristic	Symbol	LM124, LM224			LM324, A/LM2902			Unit	
		Min	Typ	Max	Min	Typ	Max		
Input offset voltage $R_S = 0\ \Omega, T_{\text{amb}} = +25^\circ\text{C}$ - (Note 4)	V_{IO}	LM324A	—	2	5	—	2	7	mV
$R_S = 0\ \Omega$ - (Note 4)		LM324A	—	—	7	—	—	9	
		LM2902	—	—	—	—	—	5 10	
Input offset current $T_{\text{amb}} = +25^\circ\text{C}$	I_{IO}	LM324A	—	3	30	—	5	50	nA
$T_{\text{min}} \leq T_{\text{amb}} \leq T_{\text{max}}$		LM324A	—	—	100	—	—	30 150	
		LM2902	—	—	—	—	—	75 200	
Input bias current $T_{\text{amb}} = +25^\circ\text{C}$ - (Note 3)	I_{IB}	LM324A	—	45	100	—	45	250	nA
$T_{\text{min}} \leq T_{\text{amb}} \leq T_{\text{max}}$		LM324A	—	40	300	—	40	100 500	
		LM324A	—	—	—	—	40	200	
Large signal voltage gain ($V_{CC} = \pm 15\text{ V}$) $T_{\text{amb}} = +25^\circ\text{C}$	A_{VD}	LM2902	50	100	—	25	100	—	V/mV
$T_{\text{min}} \leq T_{\text{amb}} \leq T_{\text{max}}, R_L = 2\text{ k}\Omega$		LM2902	25	—	—	15	—	—	
Supply voltage rejection ratio ($T_{\text{amb}} = +25^\circ\text{C}$)	LM2902	SVR	65	100	—	65	100	—	dB
Supply current ($R_L = \infty$ for all amplifiers) $T_{\text{amb}} = +25^\circ\text{C}$ $V_{CC}^+ = +30\text{ V}$ $T_{\text{min}} \leq T_{\text{amb}} \leq T_{\text{max}}$ $V_{CC}^+ = +30\text{ V}$ (except for LM2902)	I_{CC}^+, I_{CC}^-	LM2902	—	0.7	1.2	—	0.8	1.2	mA
		LM2902	—	1.5	3	—	1.5	3	
		LM2902	—	0.8	1.2	—	0.8	1.2	
Temperature coefficient of input offset voltage ($R_S = 0\ \Omega$)	αV_{IO}	LM324A	—	7	—	—	7	—	$\mu\text{V}/^\circ\text{C}$
		LM324A	—	—	—	—	7	30	
Temperature coefficient of input offset current	LM324A	αI_{IO}	—	10	—	—	10	—	$\text{pA}/^\circ\text{C}$
Input voltage range ($V_{CC}^+ = +30\text{ V}^*$) - Note 5 $T_{\text{amb}} = +25^\circ\text{C}$	V_I	LM2902	0	—	$V_{CC}^+ - 1.5$	0	—	$V_{CC}^+ - 1.5$	V
$T_{\text{min}} \leq T_{\text{amb}} \leq T_{\text{max}}$		LM2902	0	—	$V_{CC}^+ - 2$	0	—	$V_{CC}^+ - 2$	
Common-mode rejection ratio	LM324A LM2902	CMR	70	85	—	65	70	—	dB
Output short-circuit current ($T_{\text{amb}} = +25^\circ\text{C}$)	LM2902	I_{OS}	—	40	60	—	40	60	mA
Output current ($V_{CC}^+ = +15\text{ V}, V_I^+ = +1\text{ V}, V_I^- = 0\text{ V}$) $T_{\text{amb}} = +25^\circ\text{C}$	LM2902	I_O	20	40	—	20	40	—	mA
$T_{\text{min}} \leq T_{\text{amb}} \leq T_{\text{max}}$		LM2902	10	20	—	10	20	—	
Output current sink ($V_I^+ = 0\text{ V}, V_I^- = +1\text{ V}$) $V_{CC}^+ = +15\text{ V}, T_{\text{amb}} = +25^\circ\text{C}$ $V_O = +200\text{ mV}, T_{\text{amb}} = +25^\circ\text{C}$ $V_{CC}^+ = +15\text{ V}, T_{\text{min}} \leq T_{\text{amb}} \leq T_{\text{max}}$	LM2902	$I_{O(\text{sink})}$	10	20	—	10	20	—	mA
		LM2902	0.012	0.05	—	0.012	0.05	—	
		LM2902	5	8	—	5	8	—	
Output voltage swing $V_{CC}^+ = +5\text{ V}, T_{\text{amb}} = +25^\circ\text{C}, R_L \geq 2\text{ k}\Omega$ $R_L \geq 10\text{ k}\Omega$ for LM2902)	LM2902	V_{OPP}	0	—	$V_{CC}^+ - 1.5$	0	—	$V_{CC}^+ - 1.5$	V
High level output voltage ($V_{CC}^+ = +30\text{ V}^*$) $R_L = 2\text{ k}\Omega$	LM2902	V_{OH}	26	—	—	26	—	—	V
$R_L = 10\text{ k}\Omega$		LM2902	27	28	—	27	28	—	
	LM2902	V_{OH}	—	—	—	23	24	—	
Low level output voltage ($R_L \leq 10\text{ k}\Omega$)	LM2902	V_{OL}	—	5	20	—	5	20	mV
Amplifier to amplifier coupling 1 kHz $\leq f \leq 20\text{ kHz}, T_{\text{amb}} = +25^\circ\text{C}$ - (Note 6)	LM2902	—	—	-120	—	—	-120	—	dB

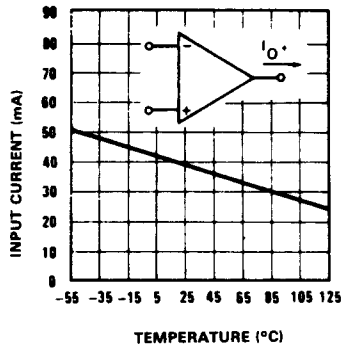
* $V_{CC}^+ = +26\text{ V}$ for LM2902

- Note 1 :** $R_{th(j-a)} = 175^{\circ}\text{C}/\text{W}$, $T_j \text{ max} = +125^{\circ}\text{C}$ (LM324) for $T_{\text{case}} = +25^{\circ}\text{C}$
 $T_j \text{ max} = +150^{\circ}\text{C}$ (LM124, 224, 2902) for $T_{\text{case}} = +50^{\circ}\text{C}$
 * $R_{th(j-a)} = 250^{\circ}\text{C}/\text{W}$, $T_j \text{ max} = +125^{\circ}\text{C}$ (LM324FP, LM2902FP) for $T_{\text{case}} = +25^{\circ}\text{C}$
 The dissipation is the total of all four amplifiers.
- Note 2 :** Short-circuits from the output to V_{CC}^{+} can cause excessive heating and eventual destruction. The maximum output current is approximately 40 mA independent of the magnitude of V_{CC}^{+} . At values of supply voltage in excess of +15 V, continuous short-circuits can exceed the power dissipation ratings and cause eventual destruction. Destructive dissipation can result from simultaneous shorts on all amplifiers.
- Note 3 :** The direction of the output current is out of the IC due to the PNP input stage. This current is essentially constant, independent of the state of the output so no loading change exists on the input lines.
- Note 4 :** $V_O = +1.4 \text{ V}$, $R_S = 0 \Omega$, $+5 \text{ V} \leq V_{CC}^{+} \leq +30 \text{ V}$, $V_{CC}^{-} = \text{Ground}$, $0 \leq V_I \leq (V_{CC}^{+} - 1.5 \text{ V})$.
- Note 5 :** The input common-mode voltage of either input signal voltage should not be allowed to go negative by more than 0.3 V. The upper end of the common-mode voltage range is $V_{CC}^{+} - 1.5 \text{ V}$, but either or both inputs can go to +32 V without damage.
- Note 6 :** Due to proximity of external components, insure that coupling is not originating via stray capacitance between these external parts. This typically can be detected as this type of capacitive coupling increases at higher frequencies.
- Note 7 :** This input current will only exist when the voltage at any of the input leads is driven negative. It is due to the collector-base junction of the input PNP transistors becoming forward biased and thereby acting as input diode clamps. In addition to this diode action, there is also lateral NPN parasitic transistor action on the IC chip. This transistor action can cause the output voltages of the op amps to go to the V_{CC}^{+} voltage level (or to ground for a large overdrive) for the time duration that an input is driven negative. This is not destructive and normal output states will re-establish when the input voltage, which was negative, again returns to a value greater than -0.3 V_{DC} .

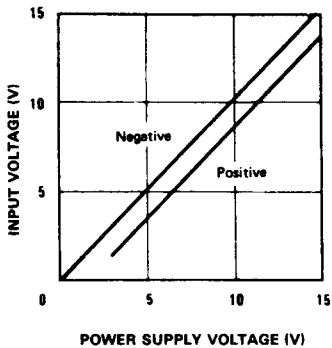
INPUT CURRENT (Note 8)



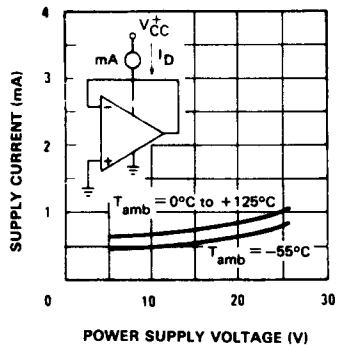
CURRENT LIMITING (Note 8)



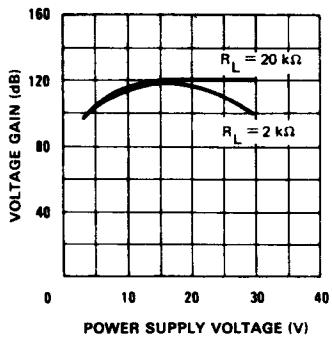
INPUT VOLTAGE RANGE



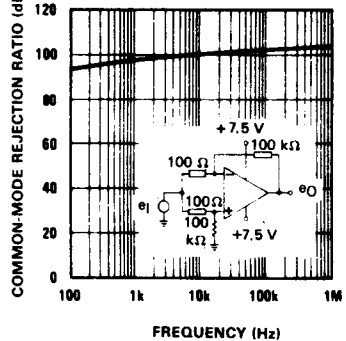
SUPPLY CURRENT



VOLTAGE GAIN

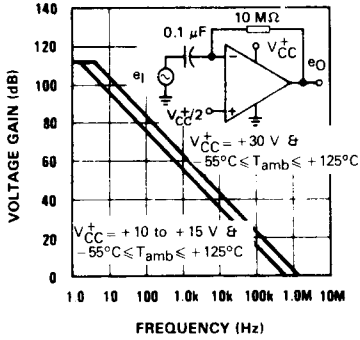


COMMON-MODE REJECTION RATIO

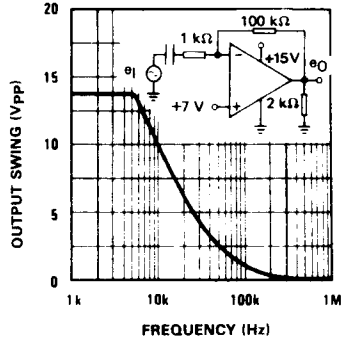


Note 8 : LM124 : $-55^\circ\text{C} \leq T_{amb} \leq +125^\circ\text{C}$
 LM224 : $-25^\circ\text{C} \leq T_{amb} \leq +85^\circ\text{C}$
 LM324, A : $0^\circ\text{C} \leq T_{amb} \leq +70^\circ\text{C}$
 LM2902 : $-40^\circ\text{C} \leq T_{amb} \leq +85^\circ\text{C}$

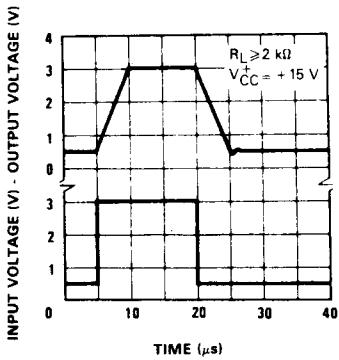
OPEN LOOP FREQUENCY RESPONSE



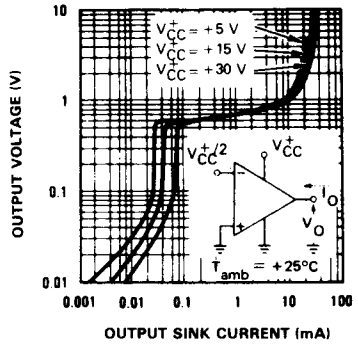
LARGE SIGNAL FREQUENCY RESPONSE



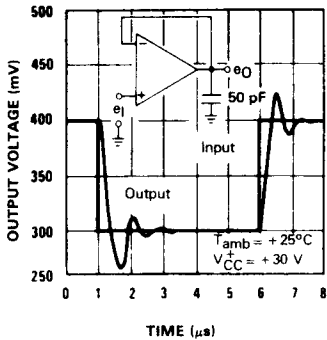
VOLTAGE FOLLOWER PULSE RESPONSE



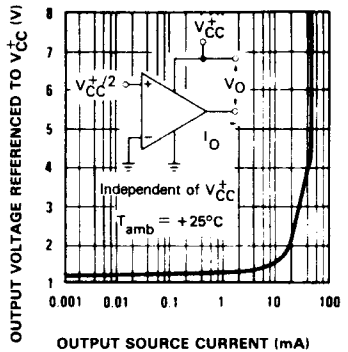
OUTPUT CHARACTERISTICS (CURRENT SINKING)

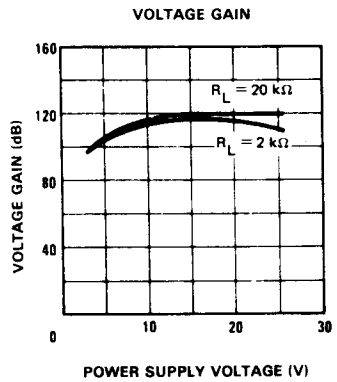
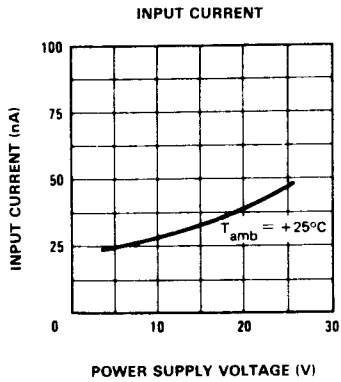


VOLTAGE FOLLOWER PULSE RESPONSE (SMALL SIGNAL)

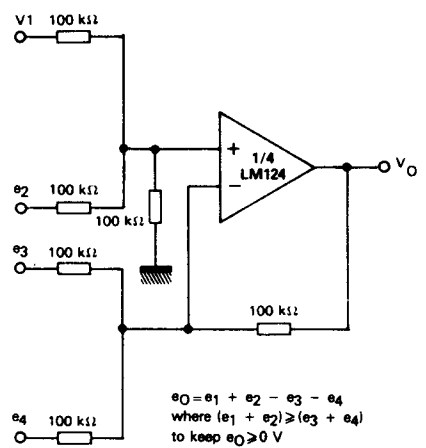
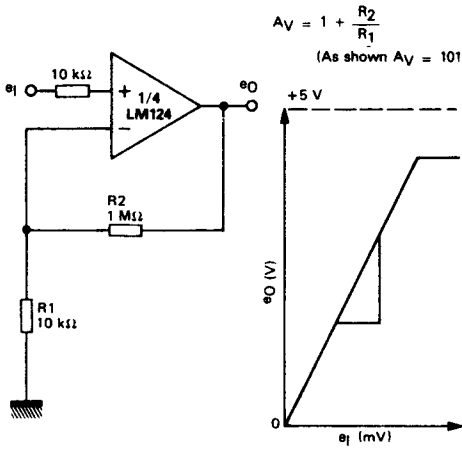
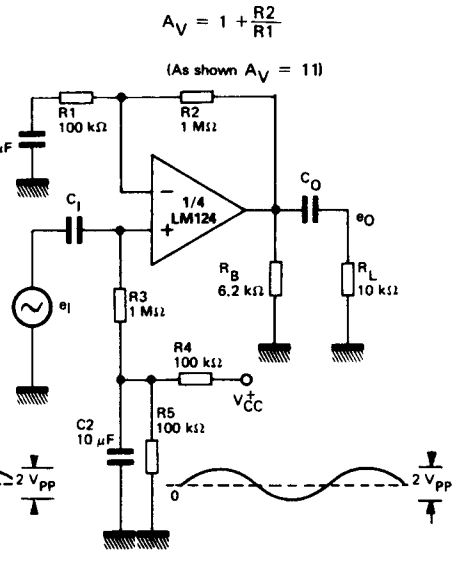
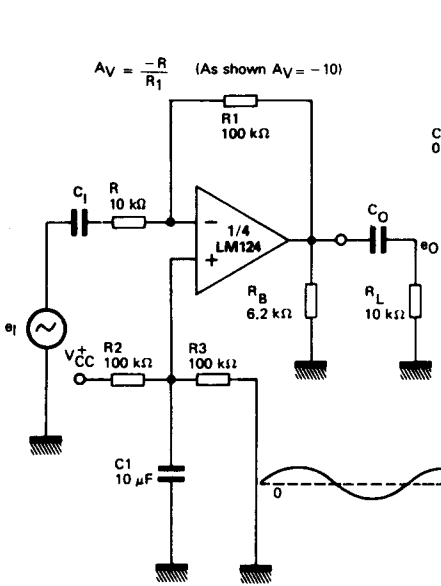


OUTPUT CHARACTERISTICS (CURRENT SOURCING)



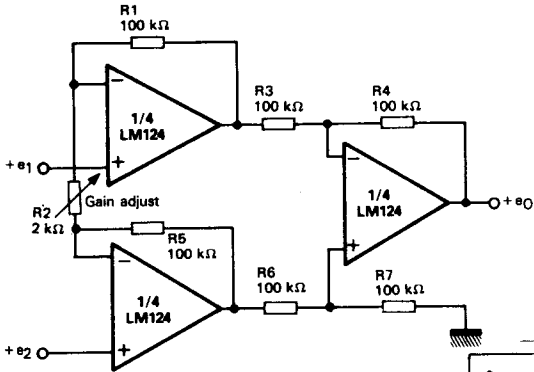


TYPICAL SINGLE - SUPPLY APPLICATIONS



TYPICAL SINGLE SUPPLY APPLICATIONS (continued)

HIGH INPUT Z ADJUSTABLE GAIN DC INSTRUMENTATION AMPLIFIER

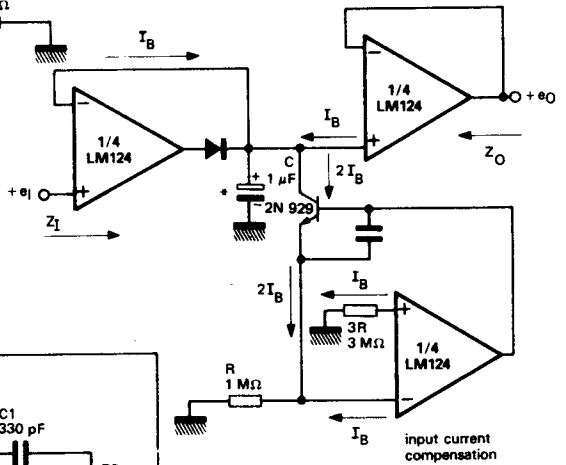


If $R_1 = R_5$ and $R_3 = R_4 = R_6 = R_7$

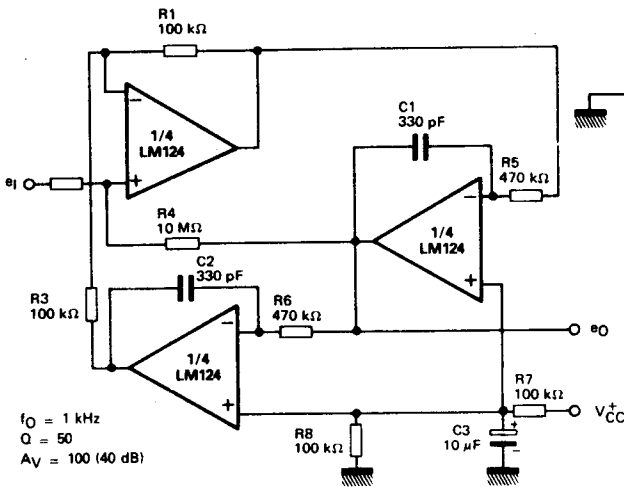
$$e_0 = \left(1 + \frac{2 R_1}{R_2} \right) (e_2 - e_1)$$

As shown $e_0 = 101 (e_2 - e_1)$

LOW DRIFT PEAK DETECTOR



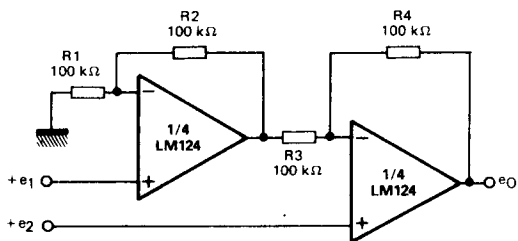
ACTIVE BANDPASS FILTER



* Polycarbonate or polyethylene

TYPICAL SINGLE - SUPPLY APPLICATIONS (continued)

HIGH INPUT Z, DC DIFFERENTIAL AMPLIFIER

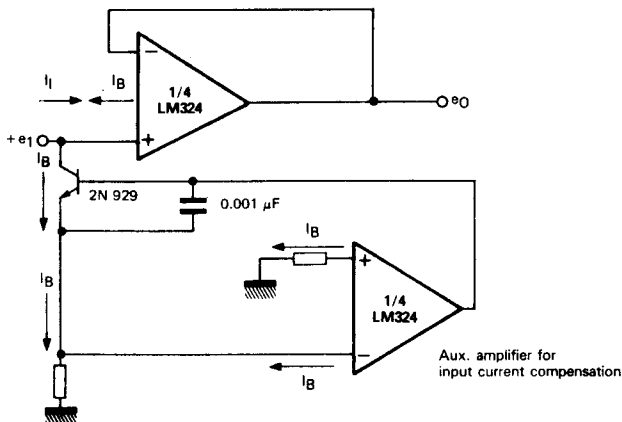


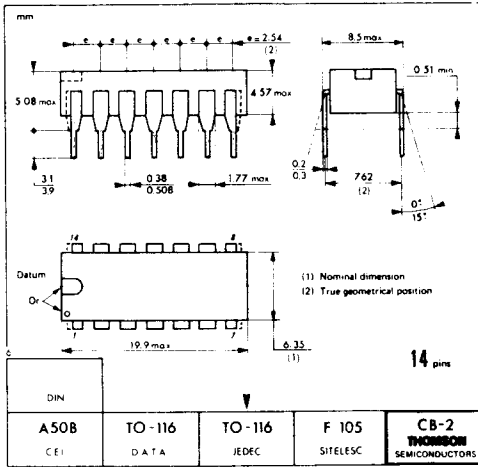
For $\frac{R_1}{R_2} = \frac{R_4}{R_3}$ (CMRR depends on this resistor ratio match)

$$e_O = \left(1 + \frac{R_4}{R_3} \right) (e_2 - e_1)$$

As shown $e_O = 2 (e_2 - e_1)$

USING SYMMETRICAL AMPLIFIERS TO REDUCE INPUT CURRENT (GENERAL CONCEPT)

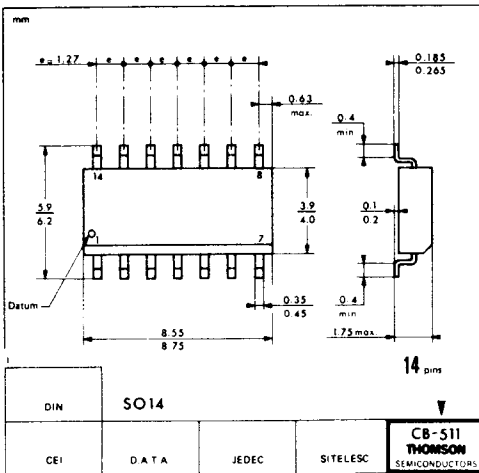




CB-2



DP SUFFIX
PLASTIC PACKAGE
DG SUFFIX
CERDIP PACKAGE



CB-511

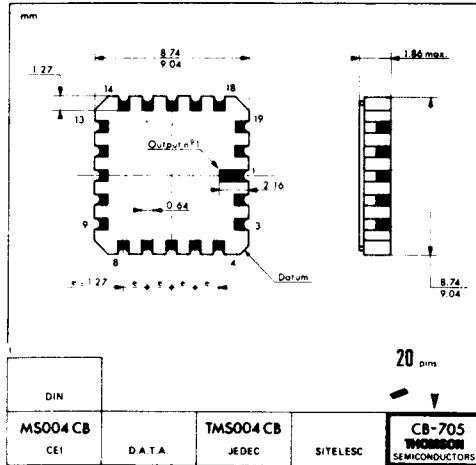


FP SUFFIX
PLASTIC MICROPACKAGE

CB-705



GC SUFFIX
TRICECOP (LCC)



These specifications are subject to change without notice.
Please inquire with our sales offices about the availability of the different packages.