

# **BUW1215**

# HIGH VOLTAGE FAST-SWITCHING NPN POWER TRANSISTOR

- STMicroelectronics PREFERRED SALESTYPE
- HIGH VOLTAGE CAPABILITY
- VERY HIGH SWITCHING SPEED

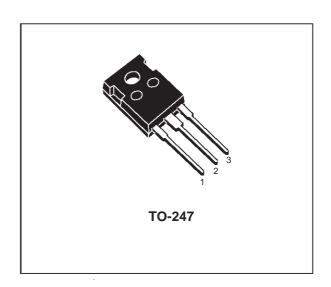
#### **APPLICATIONS:**

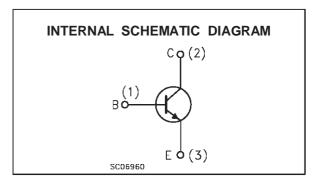
 HORIZONTAL DEFLECTION FOR COLOUR TV AND MONITORS

#### **DESCRIPTION**

The BUW1215 is manufactured using Multiepitaxial Mesa technology for cost-effective high performance and uses a Hollow Emitter structure to enhance switching speeds.

The BUH series is designed for use in horizontal deflection circuits in televisions and monitors.





#### **ABSOLUTE MAXIMUM RATINGS**

Symbol	Parameter	Value	Unit
V <sub>CBO</sub>	Collector-Base Voltage (I <sub>E</sub> = 0)	1500	V
V <sub>CEO</sub>	Collector-Emitter Voltage (I <sub>B</sub> = 0)	700	V
V <sub>EBO</sub>	Emitter-Base Voltage (I <sub>C</sub> = 0)	10	V
Ic	Collector Current	16	А
I <sub>CM</sub>	Collector Peak Current (t <sub>p</sub> < 5 ms)	22	А
I <sub>B</sub>	Base Current	9	А
I <sub>BM</sub>	Base Peak Current (t <sub>p</sub> < 5 ms)	12	А
P <sub>tot</sub>	Total Dissipation at T <sub>c</sub> = 25 °C	200	W
T <sub>stg</sub>	Storage Temperature	-65 to 150	°C
Tj	Max. Operating Junction Temperature	150	°C

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#### THERMAL DATA

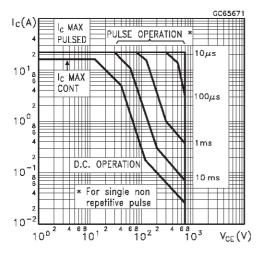
R <sub>thj-case</sub> Thermal Resistance Junction-case	Max 0.63	°C/W
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### **ELECTRICAL CHARACTERISTICS** (T<sub>case</sub> = 25 °C unless otherwise specified)

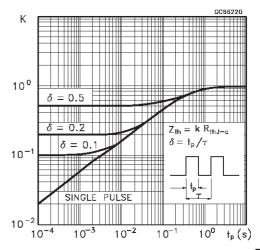
Symbol	Parameter	Test Conditions	Min.	Тур.	Max.	Unit
Ices	Collector Cut-off Current (V <sub>BE</sub> = 0)	$V_{CE} = 1500 \text{ V}$ $V_{CE} = 1500 \text{ V}$ $T_j = 125 \text{ °C}$			0.2 2	mA mA
I <sub>EBO</sub>	Emitter Cut-off Current (I <sub>C</sub> = 0)	V <sub>EB</sub> = 5 V			100	μΑ
V <sub>CEO(sus)</sub>	Collector-Emitter Sustaining Voltage	I <sub>C</sub> = 100 mA	700			V
V <sub>EBO</sub>	Emitter-Base Voltage (I <sub>C</sub> = 0)	I <sub>E</sub> = 10 mA	10			V
V <sub>CE(sat)</sub> *	Collector-Emitter Saturation Voltage	I <sub>C</sub> = 12 A I <sub>B</sub> = 2.4 A			1.5	V
V <sub>BE(sat)</sub> *	Base-Emitter Saturation Voltage	$I_C = 12 \text{ A}$ $I_B = 2.4 \text{ A}$			1.5	V
h <sub>FE</sub> *	DC Current Gain	$I_C = 12 \text{ A}$ $V_{CE} = 5 \text{ V}$ $I_C = 12 \text{ A}$ $V_{CE} = 5 \text{ V}$ $T_j = 100 ^{\circ}\text{C}$	7 5	10	14	
t <sub>s</sub>	RESISTIVE LOAD Storage Time Fall Time	$V_{CC} = 400 \text{ V}$ $I_{C} = 12 \text{ A}$ $I_{B1} = 2 \text{ A}$ $I_{B2} = -6 \text{ A}$		1.5 110		μs ns
t <sub>s</sub>	INDUCTIVE LOAD Storage Time Fall Time	$\begin{array}{lll} I_{C} = 12 \text{ A} & f = 31250 \text{ Hz} \\ I_{B1} = 2 \text{ A} & I_{B2} = -1.5 \text{ A} \\ V_{\text{ceflyback}} = 1050 \sin\!\left(\!\frac{\pi}{5}10^{6}\!\right)\!t & V \end{array}$		4 220		μs ns
t <sub>s</sub>	INDUCTIVE LOAD Storage Time Fall Time	$I_{C} = 6 \text{ A}$ $f = 64 \text{ KHz}$ $I_{B1} = 1 \text{ A}$ $V_{BE(off)} = -2 \text{ A}$ $V_{ceflyback} = 1200 \sin\left(\frac{\pi}{5} \cdot 10^{6}\right) \text{t}$ $V$		3.5 180		μs ns

\* Pulsed: Pulse duration = 300 μs, duty cycle 1.5 %

#### Safe Operating Area

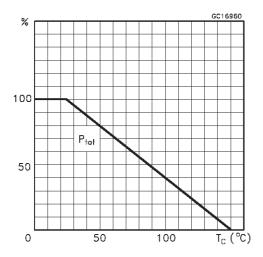


#### Thermal Impedance

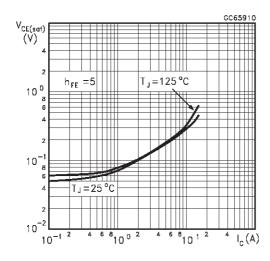


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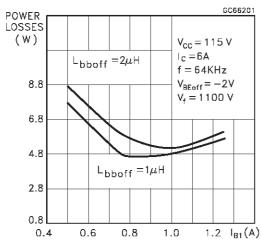
#### **Derating Curve**



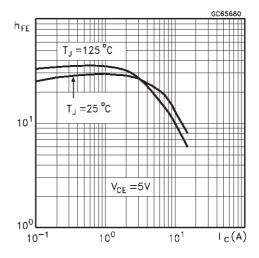
#### Collector Emitter Saturation Voltage



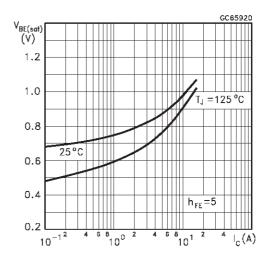
#### Power Losses at 64 KHz



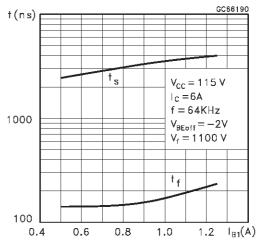
#### DC Current Gain



Base Emitter Saturation Voltage

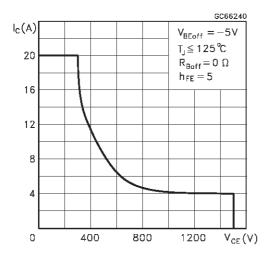


# Switching Time Inductive Load at 64 KHz (see figure 2)



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#### Reverse Biased SOA



#### **BASE DRIVE INFORMATION**

In order to saturate the power switch and reduce conduction losses, adequate direct base current  $I_{B1}$  has to be provided for the lowest gain  $h_{FE}$  at 100  $^{\circ}$ C (line scan phase). On the other hand, negative base current  $I_{B2}$  must be provided the transistor to turn off (retrace phase).

Most of the dissipation, especially in the deflection application, occurs at switch-off so it is essential to determine the value of  $I_{B2}$  which minimizes power losses, fall time  $t_f$  and, consequently,  $T_j$ . A new set of curves have been defined to give total power losses,  $t_s$  and  $t_f$  as a function of  $I_{B1}$  at 64 KHz scanning frequencies for choosing the

optimum negative drive. The test circuit is illustrated in figure 1.

The values of L and C are calculated from the following equations:

$$\frac{1}{2}L(I_{C})^{2} = \frac{1}{2}C(V_{CEfly})^{2}$$

$$\omega = 2 \pi f = \frac{1}{\sqrt{L C}}$$

Where  $I_C$  = operating collector current,  $V_{CEfly}$ = flyback voltage, f= frequency of oscillation during retrace.

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Figure 1: Inductive Load Switching Test Circuits.

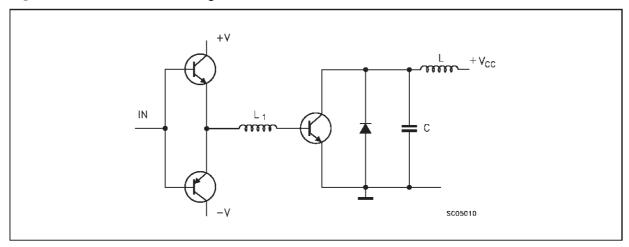
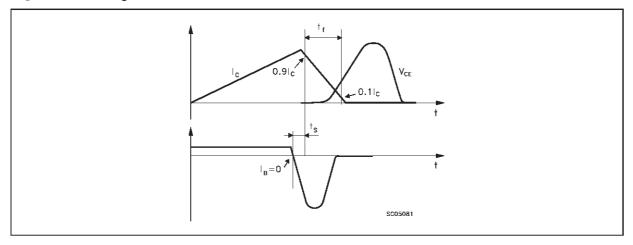
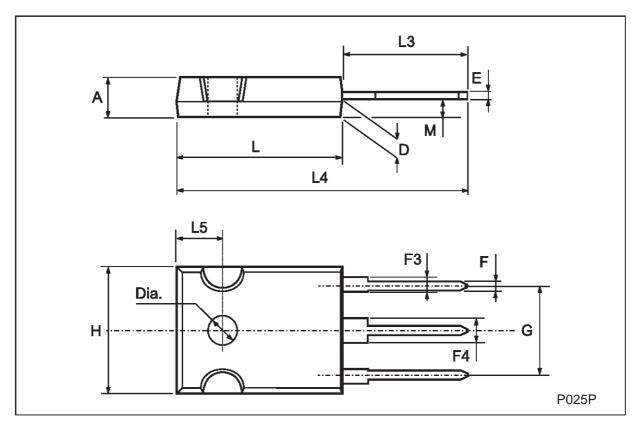


Figure 2: Switching Waveforms in a Deflection Circuit



## **TO-247 MECHANICAL DATA**

DIM.		mm			inch	
	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.
А	4.7		5.3	0.185		0.209
D	2.2		2.6	0.087		0.102
E	0.4		0.8	0.016		0.031
F	1		1.4	0.039		0.055
F3	2		2.4	0.079		0.094
F4	3		3.4	0.118		0.134
G		10.9			0.429	
Н	15.3		15.9	0.602		0.626
L	19.7		20.3	0.776		0.779
L3	14.2		14.8	0.559		0.582
L4		34.6			1.362	
L5		5.5			0.217	
М	2		3	0.079		0.118



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