Comlinear
A National Semiconductor Company

Wideband, Low-Noise, Voltage-Feedback Op Amp

CLC426

APPLICATIONS:

- Active Filters & Integrators
- Ultrasound
- Low-Power Portable Video
- ADC/DAC Buffer
- Wide Dynamic Range Amp
- Differential Amps
- Pulse/RF Amp

FEATURES:

- Wide Gain-Bandwidth product: 230MHz
- Ultra-Low Input Voltage Noise: 1.6nV/√Hz
- Very Low Harmonic Distortion: -62/-68dBc
- Fast Slew Rate: 400V/µs
- Adjustable Supply Current
- Dual ±2.5 to ±5V or Single 5 to 12V Supplies
- Externally Compensatable

DESCRIPTION

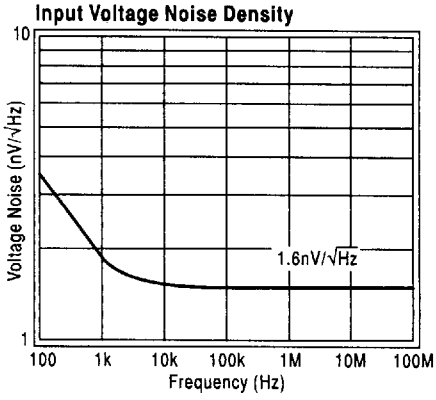
The CLC426 combines an enhanced voltage-feedback architecture with an advanced complementary bipolar process to provide a high-speed op amp with very low noise (1.6nV/√Hz & 2.0pA/√Hz) and distortion (-62/-68dBc 2nd/3rd harmonics at $1V_{pp}$ and 10MHz).

Providing a wide 230MHz gain-bandwidth product, a fast 400V/µs slew rate and very quick 16ns settling time to 0.05% , the CLC426 is the ideal choice for high speed applications requiring a very wide-dynamic range such as an input buffer for high-resolution analog-to-digital converters.

The CLC426 is internally compensated for gains ≥ 2V/V and can easily be externally compensated for unity-gain stability in applications such as wideband low-noise integrators. The CLC426 is also equipped with external supply current adjustment which allows the user to optimize power, bandwidth, noise and distortion performance for each application.

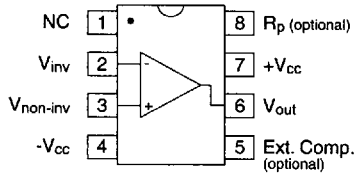
The CLC426's combination of speed, low noise and distortion and low dc errors will allow high-speed signal conditioning applications to achieve the highest signal-to-noise performance. To reduce design times and assist board layout, the CLC426 is supported by an evaluation board and SPICE simulation model available from Comlinear.

For even higher gain-bandwidth voltage-feedback op amps see the 1.9GHz CLC425 ($A_v \geq 10V/V$) or the 5.0GHz CLC422 ($A_v \geq 30V/V$).

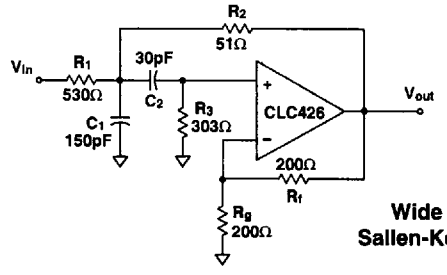


PINOUT

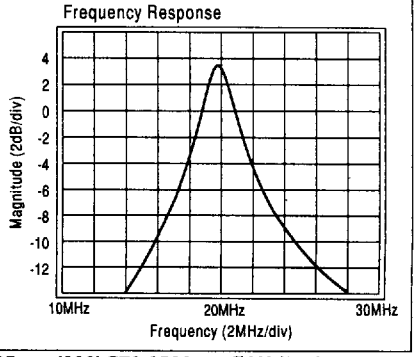
DIP & SOIC



TYPICAL APPLICATION



Wide Dynamic Range Sallen-Key Band Pass Filter 2nd-Order
(20MHz, Q=10, G=2)



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CLC426 Electrical Characteristics (V_{CC} = ±5V; A_V = +2V/V; R_f =100Ω; R_L = 100Ω; unless noted)

PARAMETERS	CONDITIONS	TYP	GUARANTEED MIN/MAX			UNITS	NOTES
Ambient Temperature	CLC426	+25°C	+25°C	0 to +70°C	-40 to +85°C		
FREQUENCY DOMAIN RESPONSE							
gain bandwidth product	V_{out} < 0.5V_{pp}	230	170	120	100	MHz	
-3dB bandwidth, A_V=+2	V_{out} < 0.5V_{pp}	130	90	70	55	MHz	B,1,4
	V_{out} < 5.0V_{pp}	50	25	22	20	MHz	
gain flatness	V_{out} < 0.5V_{pp}						
peaking	DC to 200MHz	0.6	1.5	2.2	2.5	dB	B,4
rolloff	DC to 30MHz	0.0	0.6	1.0	1.0	dB	B,4
linear phase deviation	DC to 30MHz	0.2	1.0	1.5	1.5	°	
TIME DOMAIN RESPONSE							
rise and fall time	1V step	2.3	3.5	5.0	6.5	ns	
settling time	2V step to 0.05%	16	20	24	24	ns	
overshoot	1V step	5	15	15	18	%	
slew rate	5V step	400	300	275	250	V/µs	
DISTORTION AND NOISE RESPONSE							
2nd harmonic distortion	1V_{pp}, 10MHz	- 62	- 52	- 47	- 45	dBc	B
3rd harmonic distortion	1V_{pp}, 10MHz	- 68	- 58	- 54	- 54	dBc	B
equivalent input noise	op amp only						
voltage	1MHz to 100MHz	1.6	2.0	2.3	2.6	nV/√Hz	
current	1MHz to 100MHz	2.0	3.0	3.6	4.6	pA/√Hz	
STATIC DC PERFORMANCE							
open-loop gain	DC	64	60	54	54	dB	
input offset voltage		1.0	2.0	2.8	2.8	mV	A
average drift		3	---	10	10	µV/°C	
input bias current		5	25	40	65	µA	A
average drift		90	---	600	700	nA/°C	
input offset current		0.3	3	5	5	µA	A
average drift		5	---	25	50	nA/°C	
power-supply rejection ratio	DC	73	65	60	60	dB	B
common-mode rejection ratio	DC	70	62	57	57	dB	
supply current	pin #8 open, R_L= ∞	11	12	13	15	mA	A
MISCELLANEOUS PERFORMANCE							
input resistance	common-mode	500	250	125	125	kΩ	
	differential-mode	750	200	50	25	kΩ	
input capacitance	common-mode	2.0	3.0	3.0	3.0	pF	
	differential-mode	2.0	3.0	3.0	3.0	pF	
output resistance	closed loop	0.07	0.1	0.2	0.2	Ω	
output voltage range	R_L= ∞	± 3.8	± 3.5	± 3.3	± 3.3	V	
	R_L=100Ω	± 3.5	± 3.2	± 2.6	± 1.3	V	
input voltage range	common mode	± 3.7	± 3.5	± 3.3	± 3.3	V	
output current		± 80	± 50	± 40	+ 35, -20	mA	

Absolute Maximum Ratings

supply voltage	±7V
short circuit current	(note 2)
common-mode input voltage	±V_{cc}
differential input voltage	±10V
maximum junction temperature	+200°C
storage temperature	-65°C to+150°C
lead temperature (soldering 10 sec)	+300°C

Ordering Information

Model	Temperature Range	Description
CLC426AJP	-40°C to +85°C	8-pin PDIP
CLC426AJE	-40°C to +85°C	8-pin SOIC
CLC426ALC	-40°C to +85°C	dice
CLC426AIB	-40°C to +85°C	8-pin CerDIP
CLC426A8B*	-55°C to +125°C	8-pin CerDIP, MIL-STD-883
CLC426AMC*	-55°C to +125°C	dice, MIL-STD-883
CLC426SMD*	-55°C to +125°C	DESC SMD #

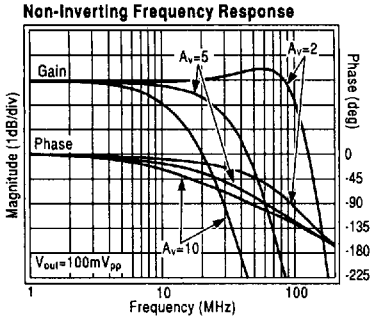
*See CLC426MIL-883 Data Sheet for Specifications

Notes

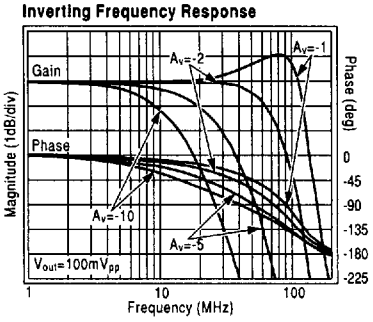
A) J-level: spec is 100% tested at +25°C, sample tested at +85°C.
L-level: spec is 100% wafer probed at 25°C.
B) J-level: spec is sample tested at 25°C.
1) Minimum stable gain with out external compensation is +2 or -1V/V, the CLC426 is unity-gain stable with external compensation.
2) Output is short circuit protected to ground, however maximum reliability is obtained if output current does not exceed 200mA.
3) See text for compensation techniques
4) Spec is guaranteed to 0.5Vpp but tested with 0.1Vpp.

CLC426 Typical Performance (T_A=25°C, $\pm V_{CC}$=±5V, A_V=+2, R_f=100Ω, R_L=100Ω, unless noted)

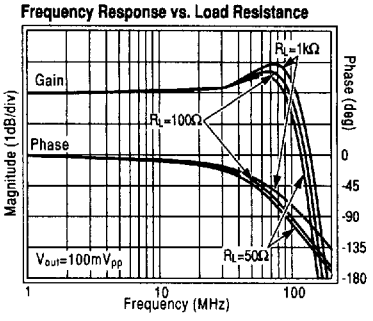
Non-Inverting Frequency Response



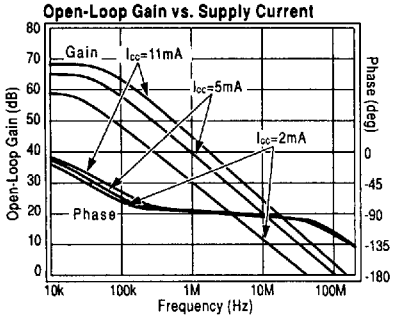
Inverting Frequency Response



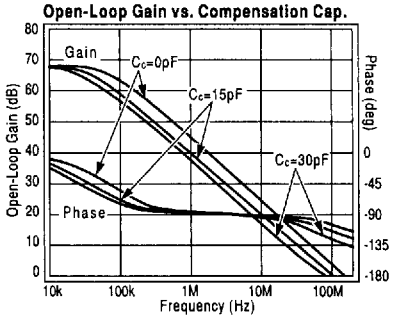
Frequency Response vs. Load Resistance



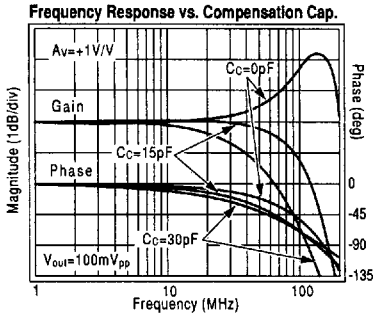
Open-Loop Gain vs. Supply Current



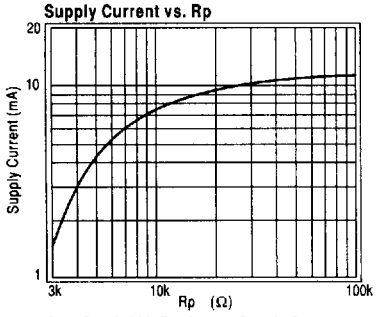
Open-Loop Gain vs. Compensation Cap.



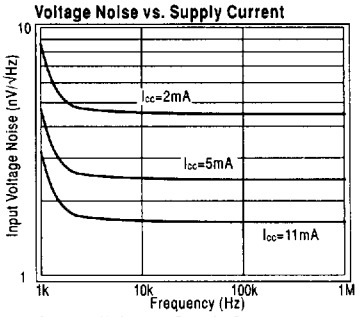
Frequency Response vs. Compensation Cap.



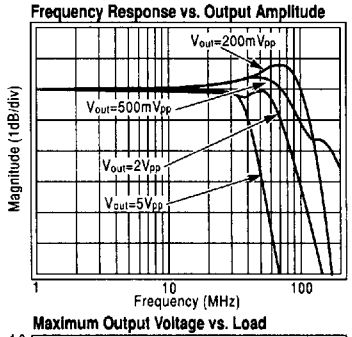
Supply Current vs. Rp



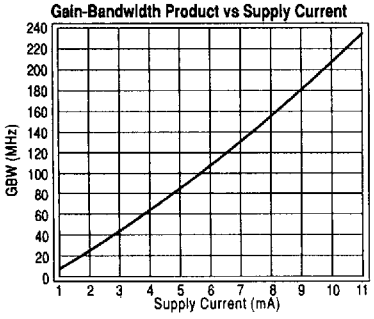
Voltage Noise vs. Supply Current



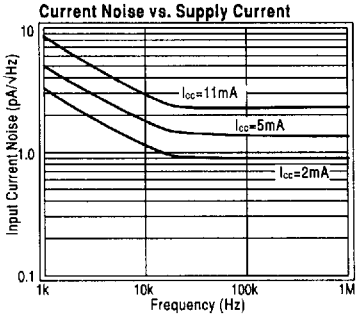
Frequency Response vs. Output Amplitude



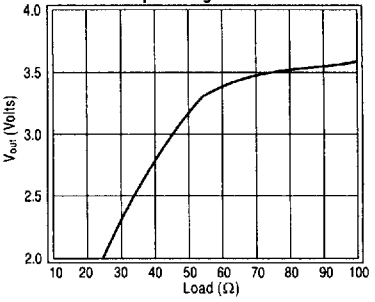
Gain-Bandwidth Product vs Supply Current



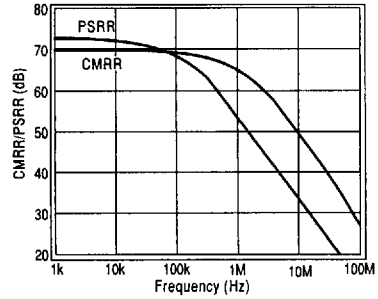
Current Noise vs. Supply Current



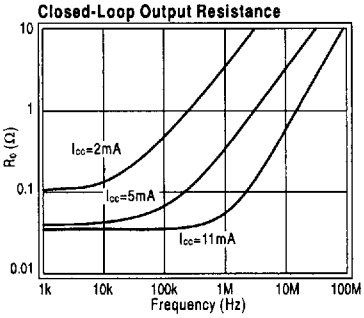
Maximum Output Voltage vs. Load



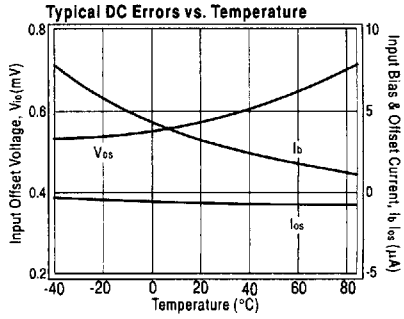
CMRR and PSRR



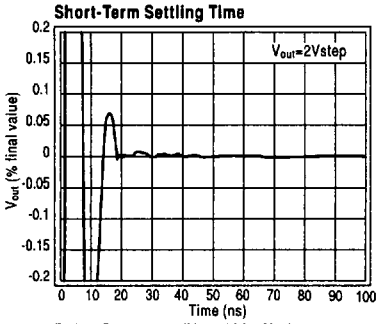
Closed-Loop Output Resistance

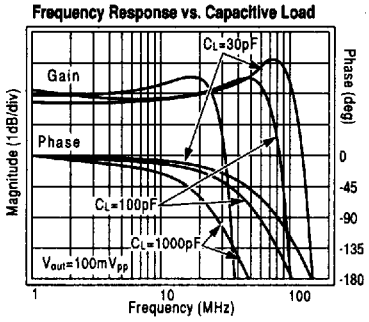


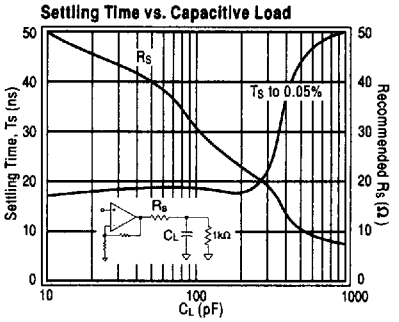
Typical DC Errors vs. Temperature

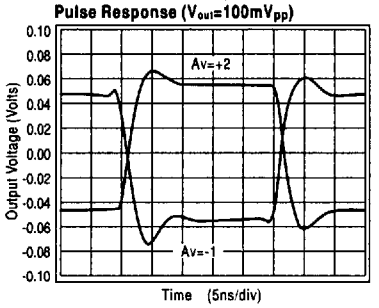


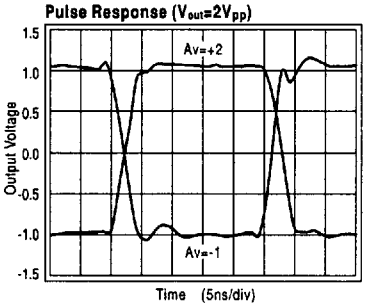
CLC426 Typical Performance (T_A=25 C, $\pm V_{CC}$=±5V, A_V=+2, R_f=100Ω, R_L=100Ω, unless noted)

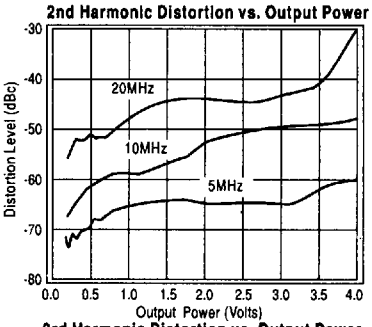


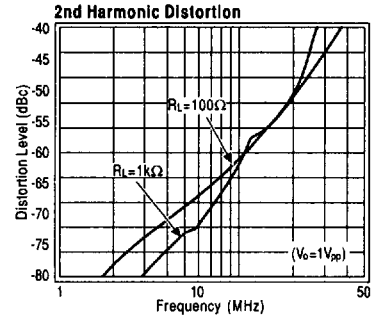


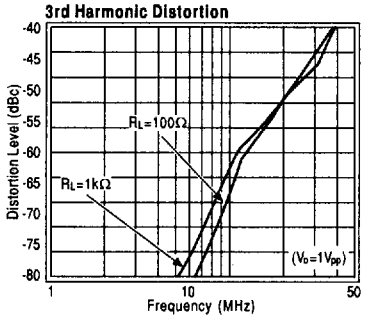


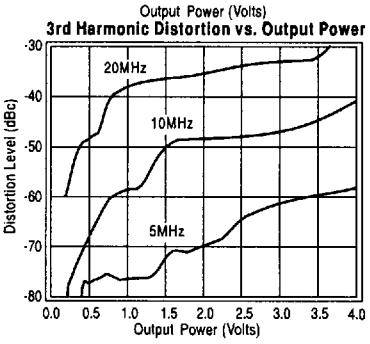












Application Discussion

Introduction

The CLC426 is a wide bandwidth voltage-feedback operational amplifier that is optimized for applications requiring wide dynamic range. The CLC426 features adjustable supply current and external compensation for the added flexibility of tuning its performance for demanding applications. The Typical Performance section illustrates many of the performance trade-offs. Although designed to operate from ±5Volt power supplies, the CLC426 is equally impressive operating from a single +5V supply. The following discussion will enable the proper selection of external components for optimum device performance in a variety of applications.

External Compensation

The CLC426 is stable for noise gains ≥2V/V. For unity-gain operation, the CLC426 requires an external compensation capacitor (from pin 5 to ground). The plot located in the Typical Performance section labeled "Frequency Response vs Compensation Cap." illustrates the CLC426's typical AC response for different values of compensation capacitor. From the plot it is seen that a value of 15pF produces the optimal response of the CLC426 at unity gain. The plot labeled "Open-Loop Gain vs. Compensation Cap." illustrates the CLC426's open-loop behavior for various values of compensation capacitor. This plot also illustrates one technique of bandlimiting the device by reducing the open-loop gain resulting in lower closed-loop bandwidth. Fig. 1 shows the effect of external compensation on the CLC426's pulse response.

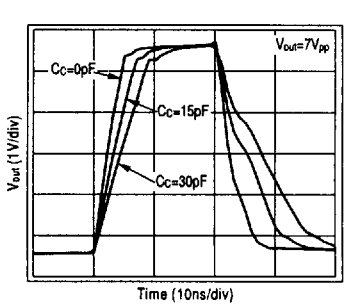


Fig. 1

Supply Current Adjustment

The CLC426's supply current can be externally adjusted downward from its nominal value to less than 2mA by adding an optional resistor (R_p) between pin 8 and the negative supply as shown in fig 2. The plot labeled "Open-Loop Gain vs. Supply Current" illustrates the influence that supply current has over the CLC426's

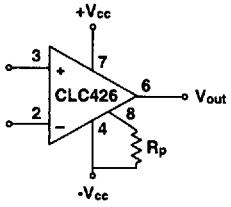


Fig. 2

open-loop response. From the plot it is seen that the CLC426 can be compensated for unity-gain stability by simply lowering its supply current. Therefore lowering the CLC426's supply current effectively reduces its open-loop gain to the point that there is adequate phase margin at unity gain crossover. The plot labeled "Supply Current vs. R_p" provides the means for selecting the value of R_p that produces the desired supply current. The curve in the plot represents nominal processing but a ±12% deviation over process can be expected. The two plots labeled "Voltage Noise vs. Supply Current" and "Current Noise vs. Supply Current" illustrate the CLC426 supply current's effect over its input-referred noise characteristics.

Driving Capacitive Loads

The CLC426 is designed to drive capacitive loads with the addition of a small series resistor placed between the

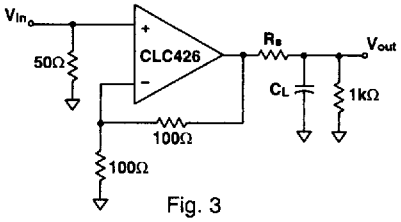


Fig. 3

output and the load as seen in fig. 3. Two plots located in the Typical Performance section illustrate this technique for both frequency domain and time domain applications. The plot labeled "Frequency Response vs. Capacitive Load" shows the CLC426's resulting AC response to various capacitive loads. The values of R_S in this plot were chosen to maximize the CLC426's AC response (limited to ≤1dB peaking).

The second plot labeled "Settling Time vs. Capacitive Load" provides the means for the selection of the value of R_S which minimizes the CLC426's settling time. As seen from the plot, for a given capacitive load R_S is chosen from the curve labeled "R_S". The resulting settling time to 0.05% can then be estimated from the curve labeled "T_S to 0.05%". The plot of fig. 4 shows the CLC426's pulse response for various capacitive loads

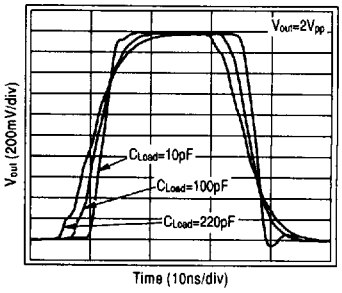


Fig. 4

where R_S has been chosen from the plot labeled "Settling Time vs. Capacitive Load".

Faster Settling

The circuit of fig. 5 shows an alternative method for driving capacitive loads that results in quicker settling times. The small series-resistor, R_S, is used to decouple the CLC426's open-loop output resistance, R_{out}, from

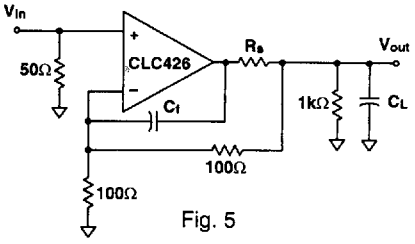


Fig. 5

the load capacitance. The small feedback-capacitance, C_f, is used to provide a high-frequency bypass between the output and inverting input. The phase lead introduced by C_f compensates for the phase lag due to C_L and therefore restores stability. The following equations provide values of R_S and C_f for a given load capacitance and closed-loop amplifier gain.

$$R_s = R_{out}\left(\frac{R_f}{R_g}\right); \quad \text{where } R_{out} \approx 6\Omega \qquad \text{Eq. 1}$$

$$C_f = \left(1+\left(\frac{R_f}{R_g}\right)\right)^2 C_L\left(\frac{R_{out}}{R_g}\right) \qquad \text{Eq. 2}$$

The plot in fig. 6 shows the result of the two methods of capacitive load driving mentioned above while driving a 100pF||1kΩ load.

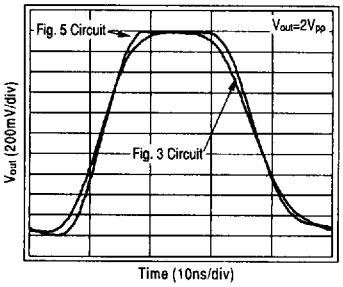


Fig. 6

Single-Supply Operation

The CLC426 can be operated with single power supply as shown in fig. 7. Both the input and output are capacitively coupled to set the dc operating point.

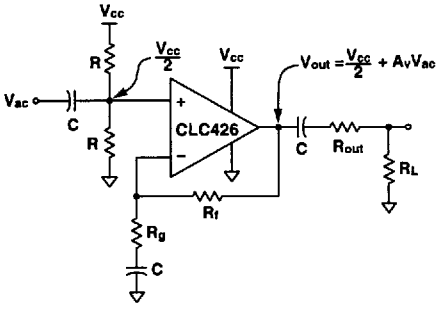


Fig. 7

DAC Output Buffer

The CLC426's quick settling, wide bandwidth and low differential input capacitance combine to form an excellent I-to-V converter for current-output DACs in such applications as reconstruction video. The circuit of fig. 8 implements a low-noise transimpedance amplifier commonly used to buffer high-speed current output devices. The transimpedance gain is set by R_f. A feedback capacitor, C_f, is needed in order to compensate for the inductive behavior of the closed-loop frequency response of this type of circuit. Equation 3 shows a means of calculating the value of C_f which will provide conditions for a maximally-flat signal frequency response with approximately 65° phase margin and 5% step-response overshoot. Notice that C_t is the sum of the DAC output capacitance and the differential input capacitance of the CLC426 which is located in its Electrical Characteristics Table. Notice also that CLC426's gain-bandwidth product (GBW) is also located in the same table. Equation 5 provides the resulting signal bandwidth.

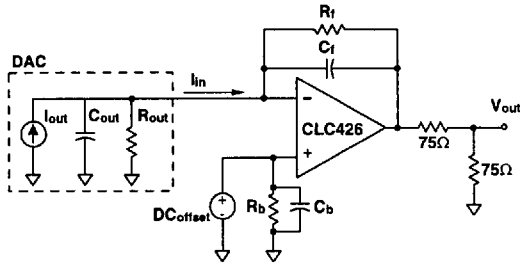


Fig. 8

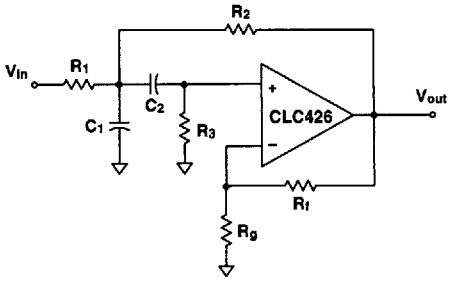
$$C_f = 2\sqrt{\frac{C_t}{2\pi R_f GBW}} \qquad \text{Eq. 3}$$

$$C_t = C_{out} + C_{in\,dif} \qquad \text{Eq. 4}$$

$$\text{signal bandwidth} = \frac{1}{2}\sqrt{\frac{GBW}{2\pi R_f C_t}} \qquad \text{Eq. 5}$$

Sallen-Key Active Filters

The CLC426 is well suited for Sallen-Key type of active filters. Fig. 9 shows the 2nd order Sallen-Key band-pass filter topology and design equations.



$$C_2 = \frac{1}{5}C_1$$

$$G = 1 + \frac{R_f}{R_g}, \text{ desired mid-band gain}$$

$$R_1 = 2\frac{Q}{GC_1(2\pi f)}, \text{ where f = desired center frequency}$$

$$R_2 = \frac{GR_1\left(\sqrt{1+4.8Q^2-2G+G^2}+1\right)}{4.8Q^2-2G+G^2}$$

$$R_3 = \frac{5GR_1\left(\sqrt{1+4.8Q^2-2G+G^2}+G-1\right)}{4Q^2}$$

Fig. 9

To design the band-pass, begin by choosing values for R_f and R_g, for example $R_f = R_g = 200\Omega$. Then choose reasonable values for C_1 and C_2 (where C_1=5C_2) and then compute R_1. R_2 and R_3 can then be computed. For optimum high-frequency performance it is recommended that the resistor values fall in the range of 10Ω to 1kΩ and the capacitors be kept above 10pF. The design can be further improved by compensating for the delay through the op amp. For further details on this technique, please request Application Note OA-21 from Comlinear Corporation.

Printed Circuit Board Layout

Generally, a good high-frequency layout will keep power supply and ground traces away from the inverting input and output pins. Parasitic capacitances on these nodes to ground will cause frequency-response peaking and possible circuit oscillation, see OA-15 for more information. Comlinear suggests the 730013 (through-hole) or the 730027 (SOIC) evaluation board as a guide for high-frequency layout and as an aid in device testing and characterization.