

## THS6226A Gated-Class H, Dual-Port VDSL2 Line Driver

### 1 Features

- Digitally-Adjustable Quiescent Current: 9.4 mA to 24.8 mA
- Bias Current Step: 1.0 mA
- Independent Voltage Boost and Main Line Driver Disable
- Low-Power Line Termination Mode
- Full Capacitor Recharge: 200  $\mu$ s
- Low Input Voltage Noise Density: 6.5 nV/ $\sqrt{\text{Hz}}$  Input-Referred Voltage Noise
- Low MTPR Distortion: 70 dB with +19.8 dBm G.993.2—Profile 8b
- 83-dBc HD3 (1 MHz, 60- $\Omega$  Differential)
- High Output Current: 383 mA into 60  $\Omega$
- Wide Output Swing: 40 V<sub>PP</sub> (+12-V, 60- $\Omega$  Differential Load with a 1:1.4 Transformer)
- Wide Bandwidth: 97 MHz
- Port-to-Port Separation: 90 dB at 1 MHz
- PSRR: 70 dB at 1 MHz for Good Isolation

### 2 Applications

- Ideal for All VDSL2 Profiles
- Backwards-Compatible with ADSL, ADSL2+, and ADSL2++ Systems

### 3 Description

The THS6226A is a dual-port, class H, current-feedback architecture, differential line driver amplifier system ideal for xDSL systems. The device is targeted for use in very-high-bit-rate digital subscriber line 2 (VDSL2) line driver systems that enable native DTM signals while supporting greater than 20.5-dBm line power (up to 8.5 MHz) with good linearity, supporting the G.993.2 VDSL2 8b profile. The device is also fast enough to support central-office transmissions of 14.5-dBm line power up to 30 MHz.

The unique architecture of the device allows quiescent current to be minimal while still achieving very high linearity. Differential distortion, under full bias conditions, is –91 dBc at 1 MHz and reduces to only –75 dBc at 5 MHz. Fixed multiple bias settings of the amplifiers offer enhanced power savings for line lengths where the full performance of the amplifier is not required. To allow for even more flexibility and power savings on all profiles, quiescent current is digitally adjustable from 7.6 mA to 23 mA with a bias current step of 1.0 mA. For systems where additional power savings while not transmitting are desired, the device can be used in its line termination mode to maintain impedance matching.

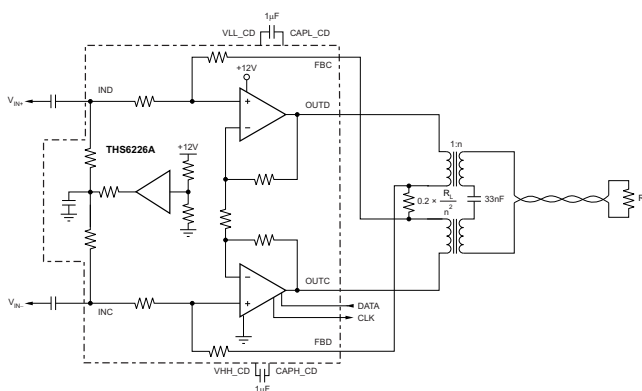
The wide output swing on 12-V power supplies, coupled with excellent current drive, allows for wide dynamic headroom, keeping distortion minimal. The device is available in a VQFN-32 PowerPAD™ package.

#### Device Information<sup>(1)</sup>

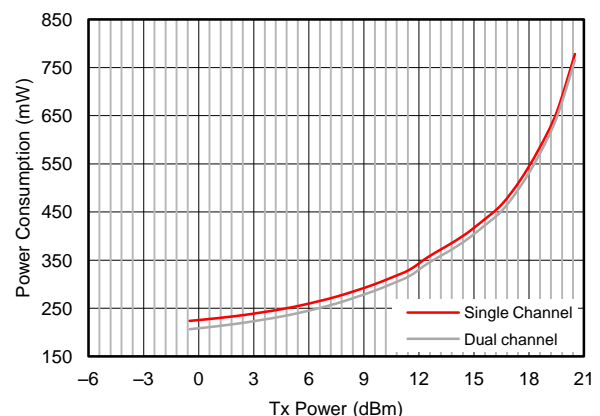
PART NUMBER	PACKAGE	BODY SIZE (NOM)
THS6226A	VQFN (32)	5.00 mm x 5.00 mm

(1) For all available packages, see the orderable addendum at the end of the datasheet.

#### Typical VDSL2 Line Driver Circuit Using One Port of the THS6226A



#### Power Consumption vs Tx



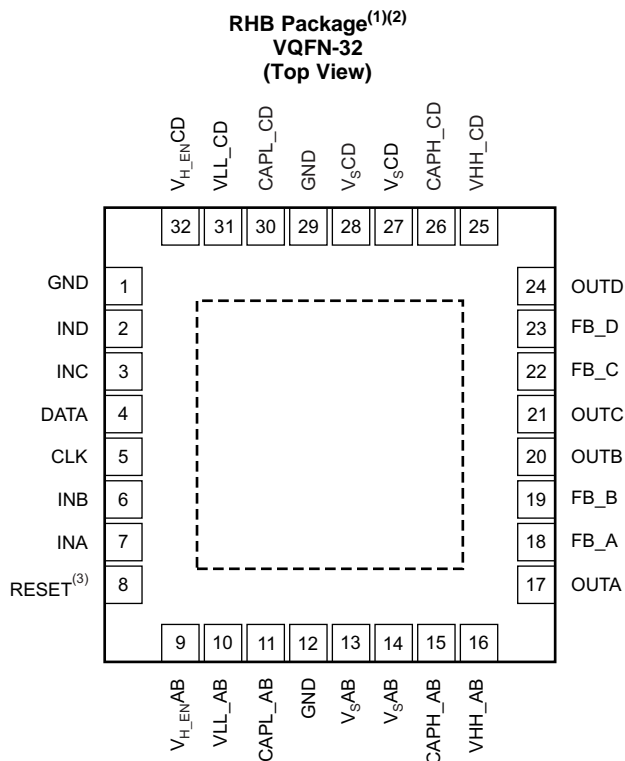
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## 4 Revision History

Changes from Original (April 2014) to Revision A	Page
• Changed HBM parameter in Handling Ratings table .....	<b>5</b>

## 5 Pin Configuration and Functions



(1) The PowerPAD is electrically isolated from all other pins and can be connected to any potential voltage range from  $V_{S-}$  to  $V_{S+}$ . Typically, the PowerPAD is connected to the GND plane because this plane tends to physically be the largest and is able to dissipate the most amount of heat.

(2) The device defaults to the disabled mode at power-up.

(3) Default is GND (internal pull-down resistor).

### Pin Functions

PIN		I/O	DESCRIPTION
NO.	NAME		
1, 12, 29	GND	—	Analog ground
2	IND	I	Input D of amplifier CD
3	INC	I	Input C of amplifier CD
4	DATA	I	Serial interface data pin
5	CLK	I	Serial interface CLK pin
6	INB	I	Input B of amplifier AB
7	INA	I	Input A of amplifier AB
8	RESET	I	Reset the internal register to 00h (startup conditions, state machine may require resetting)
9	V <sub>H_ENAB</sub>	I	Class H mode control pin for amplifier AB
10	VLL_AB	—	Amplifier AB low pump supply
11	CAPL_AB	—	Amplifier AB negative voltage pump capacitor pin
13, 14	V <sub>SAB</sub>	—	Amplifier AB supply voltage
15	CAPH_AB	—	Amplifier AB positive voltage pump capacitor pin
16	VHH_AB	—	Amplifier AB high pump supply
17	OUTA	O	Output A of amplifier AB
18	FB_A	I	Feedback for active output impedance of amplifier AB
19	FB_B	I	Feedback for active output impedance of amplifier AB
20	OUTB	O	Output B of amplifier AB
21	OUTC	O	Output C of amplifier CD
22	FB_C	I	Feedback for active output impedance of amplifier CD
23	FB_D	I	Feedback for active output impedance of amplifier CD
24	OUTD	O	Output D of amplifier CD
25	VHH_CD	—	Amplifier CD high pump supply
26	CAPH_CD	—	Amplifier CD positive voltage pump capacitor pin
27, 28	V <sub>SCD</sub>	—	Amplifier CD supply voltage
30	CAPL_CD	—	Amplifier CD negative voltage pump capacitor pin
31	VLL_CD	—	Amplifier CD low pump supply
32	V <sub>H_ENCD</sub>	I	Class H mode control pin for amplifier CD
PowerPAD		—	The PowerPAD must be connected to any internal PCB ground plane using multiple vias for good thermal performance.

## 6 Specifications

### 6.1 Absolute Maximum Ratings<sup>(1)</sup>

over operating free-air temperature range (unless otherwise noted)

		MIN	MAX	UNIT
Supply voltage, GND to $V_{S+}$	Class AB only		16.5	V
	Class H only		12.8	V
Input voltage, $V_I$			15	V
Output current, $I_O$	Static dc <sup>(2)</sup>		±100	mA
Continuous power dissipation		See <a href="#">Thermal Information</a> table		
Temperature	Maximum junction, any condition, $T_J$ <sup>(3)</sup>		150	°C
	Maximum junction, continuous operation, long-term reliability, $T_J$ <sup>(4)</sup>		130	°C

- (1) Stresses above those listed under *absolute maximum ratings* may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under *recommended operating conditions* is not implied. Exposure to absolute maximum rated conditions for extended periods may degrade device reliability.
- (2) The device incorporates a PowerPAD on the underside of the chip, which functions as a heatsink and must be connected to a thermally dissipating plane for proper power dissipation. Failure to do so may result in exceeding the maximum junction temperature, which could permanently damage the device. See the technical brief [PowerPAD™ Thermally Enhanced Package \(SLMA002\)](#) for more information about using the PowerPAD thermally-enhanced package. Under high-frequency ac operation (> 10 kHz), the short-term output current capability is much greater than the continuous dc output current rating. This short-term output current rating is roughly 8.5 times the dc capability, or approximately ±850 mA.
- (3) The absolute maximum junction temperature under any condition is limited by the constraints of the silicon process.
- (4) The absolute maximum junction temperature for continuous operation is limited by the package constraints. Operation above this temperature may result in reduced reliability or lifetime of the device.

### 6.2 Handling Ratings

		MIN	MAX	UNIT		
$T_{stg}$	Storage temperature range		-65	150	°C	
$V_{(ESD)}$	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001	Supply and ground pins with respect to PowerPad: GND (pins 1, 12, 29), $V_{SAB}$ (pins 13, 14), $V_{SCD}$ (pins 27, 28)	-1.5	1.5	kV
			All other pins	-2	2	
		Charged device model (CDM), per JEDEC specification JESD22-C101, all pins		-500	500	V

### 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
Power-supply voltage range	Class H	10		12.6	V
	Class AB	10		15	V
Operating junction temperature		–40		130	°C

### 6.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		THS6226A		UNIT
		RHB (VQFN)		
		32 PINS		
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	35.1		°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	22.1		
R <sub>θJB</sub>	Junction-to-board thermal resistance	7.0		
Ψ <sub>JT</sub>	Junction-to-top characterization parameter	0.3		
Ψ <sub>JB</sub>	Junction-to-board characterization parameter	6.9		
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	1.3		

 (1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953](http://SPRA953).

### 6.5 Electrical Characteristics: V<sub>S</sub> = +12 V

 At T<sub>A</sub> = 25°C, R<sub>MATCH</sub> = 10.2 Ω, transformer turn ratio 1:1.4, R<sub>L</sub> = 100-Ω differential at transformer output, full bias mode, and active impedance circuit configuration, unless otherwise noted. Each port is tested independently.

PARAMETER		CONDITIONS	MIN	TYP	MAX	UNIT	TEST LEVEL <sup>(1)</sup>
<b>AC PERFORMANCE</b>							
	Small-signal bandwidth, –3 dB	V <sub>O</sub> = 2 V <sub>PP</sub> , differential at OUTCD and OUTAB, gain = 19 V/V		97		MHz	C
	0.1-dB bandwidth flatness	V <sub>O</sub> = 2 V <sub>PP</sub>		30		MHz	C
	Large-signal bandwidth	V <sub>O</sub> = 7.5 V <sub>PP</sub>		80		MHz	C
SR	Slew rate (10% to 90% level)	V <sub>O</sub> = 15-V step, differential		1750		V/μs	C
	Rise-and-fall time	V <sub>O</sub> = 2 V <sub>PP</sub>		3.6		ns	C
HD2	Second-harmonic distortion	Full bias, f = 1 MHz, V <sub>O</sub> = 2 V <sub>PP</sub> , R <sub>L</sub> = 60-Ω differential		–87		dBc	C
		Full bias, f = 5 MHz, V <sub>O</sub> = 2 V <sub>PP</sub> , R <sub>L</sub> = 60-Ω differential		–73		dBc	C
HD3	Third-harmonic distortion	Full bias, f = 1 MHz, V <sub>O</sub> = 2 V <sub>PP</sub> , R <sub>L</sub> = 60-Ω differential		–83		dBc	C
		Full bias, f = 5 MHz, V <sub>O</sub> = 2 V <sub>PP</sub> , R <sub>L</sub> = 60-Ω differential		–71		dBc	C
	Differential input voltage noise	f = 1 MHz, input-referred		6.5		nV/√Hz	C
<b>DC PERFORMANCE</b>							
	Differential gain	Closed-loop configuration		19		V/V	C
	Differential gain error <sup>(2)</sup>	T <sub>A</sub> = 25°C			±8%		A
V <sub>IO</sub>	Input offset voltage	T <sub>A</sub> = 25°C		±1	±10	mV	A
		T <sub>A</sub> = –40°C to 85°C			±11	mV	B
	Input offset voltage drift				15	μV/°C	B
	Input offset voltage matching	Channels 1 to 2 and 3 to 4 only, T <sub>A</sub> = 25°C		±1	±10	mV	A
<b>INPUT CHARACTERISTICS</b>							
	Noninverting input resistance			2    2		kΩ    pF	C
	Input bias voltage	T <sub>A</sub> = 25°C	5.8	6	6.2	V	A

- (1) Test levels: **(A)** 100% tested at 25°C. Overtemperature limits set by characterization and simulation. **(B)** Limits set by characterization and simulation. **(C)** Typical value only for information.
- (2) Negative feedback loop only.

**Electrical Characteristics:  $V_S = +12\text{ V}$  (continued)**

At  $T_A = 25^\circ\text{C}$ ,  $R_{\text{MATCH}} = 10.2\ \Omega$ , transformer turn ratio 1:1.4,  $R_L = 100\text{-}\Omega$  differential at transformer output, full bias mode, and active impedance circuit configuration, unless otherwise noted. Each port is tested independently.

PARAMETER		CONDITIONS	MIN	TYP	MAX	UNIT	TEST LEVEL <sup>(1)</sup>	
<b>OUTPUT CHARACTERISTICS</b>								
Class H output	Voltage swing	$R_L = 60\text{-}\Omega$ differential, class H operation <sup>(3)(4)</sup> , each output, $T_A = 25^\circ\text{C}$	16	17.5		V	A	
			-4	-5.5		V	A	
	$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ <sup>(3)(4)</sup>		15.7			V	B	
			-3.7			V	B	
Current (sourcing, sinking)	$R_L = 60\text{-}\Omega$ differential, class H operation, $T_A = 25^\circ\text{C}$	$\pm 333$	$\pm 383$		mA	A		
	$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	$\pm 323$			mA	B		
Class AB output	Voltage swing	$R_L = 60\text{-}\Omega$ differential, normal operation <sup>(3)</sup> , each output, $T_A = 25^\circ\text{C}$	9.9	10.1		V	A	
			2.1	1.9		V	A	
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ <sup>(3)</sup>		9.8			V	B
				2.2			V	B
	Current (sourcing, sinking)	$R_L = 60\text{-}\Omega$ differential, normal operation, $T_A = 25^\circ\text{C}$	$\pm 130$	$\pm 137$		mA	A	
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	$\pm 126$			mA	B	
Short-circuit output current				1		A	C	
$z_o$	Output impedance	$f = 1\text{ MHz}$ , differential		25		$\Omega$	C	
Crosstalk		$f = 1\text{ MHz}$ , $V_{\text{OUT}} = 2\text{ V}_{\text{PP}}$ , port 1 to port 2		-90		dB	C	
<b>POWER SUPPLY</b>								
Maximum operating voltage	Class AB, $T_A = 25^\circ\text{C}$		10	12	15	V	A	
	$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$		10		15	V	B	
	Class H		10	12	12.6	V	B	
	$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$		10		12.6	V	B	
$I_Q$	Quiescent current ( $I_{S+}$ )	Per port, bias 15, class H enable (power supplies connected together), $T_A = 25^\circ\text{C}$	23.4	24.6	25.8	mA	A	
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	22.9		26.1	mA	B	
		Per port, bias 15, class H disable (power supplies connected together), $T_A = 25^\circ\text{C}$	22.8	24.0	25.2	mA	A	
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	22.3		25.7	mA	B	
		Bias current step			1		mA	C
		Per port, bias 0, class H disable (power supplies connected together), $T_A = 25^\circ\text{C}$	8.5	9.7	10.9	mA	A	
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	8.0		11.4	mA	B	
		Per port, line termination mode ( $B9 = B8 = B7 = B6 = 0$ ) (power supplies connected together)		7.0			mA	C
		Both ports, main amplifiers and class H disable ( $B9 = B8 = B7 = B6 = 0$ )		1.9	2.4		mA	A
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$			2.5		mA	B
PSRR	Power-supply rejection ratio	Differential, from 12 V, GND, $T_A = 25^\circ\text{C}$	60	70		dB	A	
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	58			dB	B	

(3) Measured at the amplifier outputs (pins 17, 20, 21, and 24).

(4) Capacitor fully charged, no droop.

**Electrical Characteristics:  $V_S = +12\text{ V}$  (continued)**

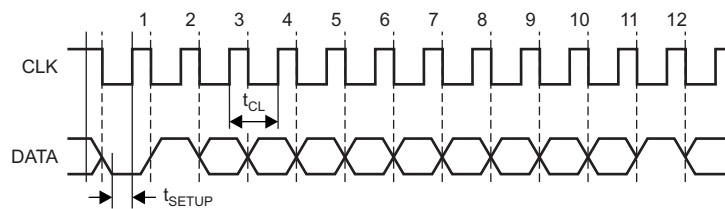
At  $T_A = 25^\circ\text{C}$ ,  $R_{MATCH} = 10.2\ \Omega$ , transformer turn ratio 1:1.4,  $R_L = 100\text{-}\Omega$  differential at transformer output, full bias mode, and active impedance circuit configuration, unless otherwise noted. Each port is tested independently.

PARAMETER		CONDITIONS	MIN	TYP	MAX	UNIT	TEST LEVEL <sup>(1)</sup>
<b>LOGIC</b>							
Logic pin	Logic threshold	Logic 1, with respect to GND <sup>(5)</sup>	1.9			V	C
		Logic 0, with respect to GND <sup>(5)</sup>			0.8	V	C
	Input Bias current	Logic X = 0.5 V (logic 0), $T_A = 25^\circ\text{C}$		10	25	$\mu\text{A}$	A
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$			30	$\mu\text{A}$	B
		Logic X = 3.3 V (logic 1), $T_A = 25^\circ\text{C}$		66	125	$\mu\text{A}$	A
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$			130	$\mu\text{A}$	B
Input impedance			50    1		k $\Omega$    pF	C	
$t_{d(on)}$	Turn-on time delay	Time for $I_S$ to reach 50% of final value		1		$\mu\text{s}$	C
$t_{d(off)}$	Turn-off time delay	Time for $I_S$ to reach 50% of final value		1		$\mu\text{s}$	C

(5) The GND pin usable range is from  $V_{S-}$  to  $(V_{S+} - 5\text{ V})$ .

**6.6 Timing Characteristics**

PARAMETER	MIN	MAX	UNITS
$t_{CL}$ Clock period	200		ns



**Figure 1. Serial Interface Timing**



### 6.7 Typical Characteristics

At  $T_A = 25^\circ\text{C}$ , 1:1.4 transformer, and 10.2- $\Omega$  matching resistance, unless otherwise noted

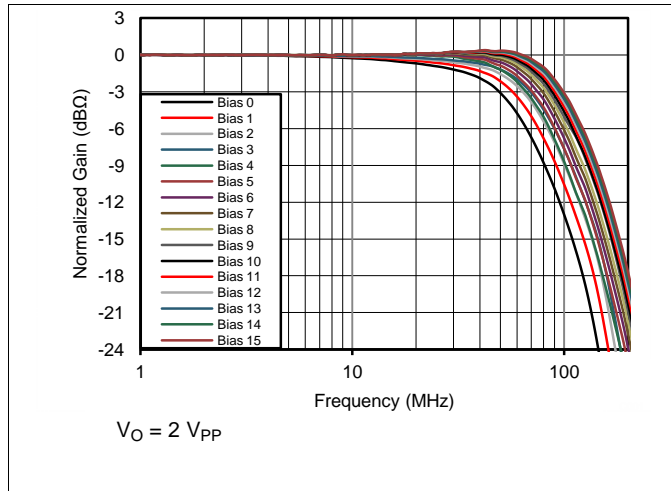


Figure 2. Normalized Small-Signal Frequency Response

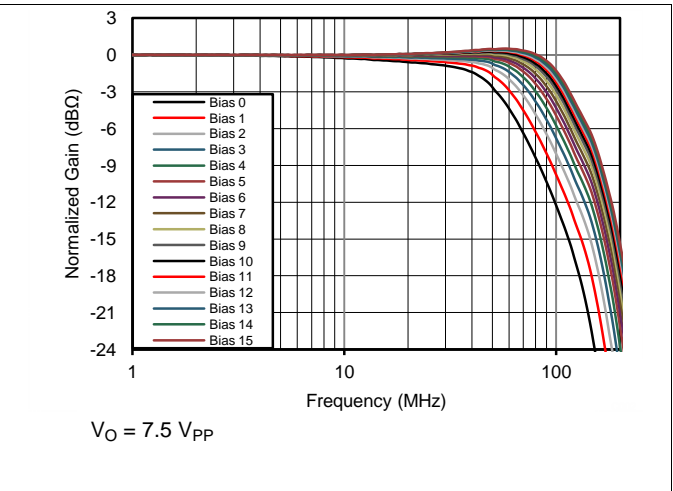


Figure 3. Normalized Large-Signal Frequency Response

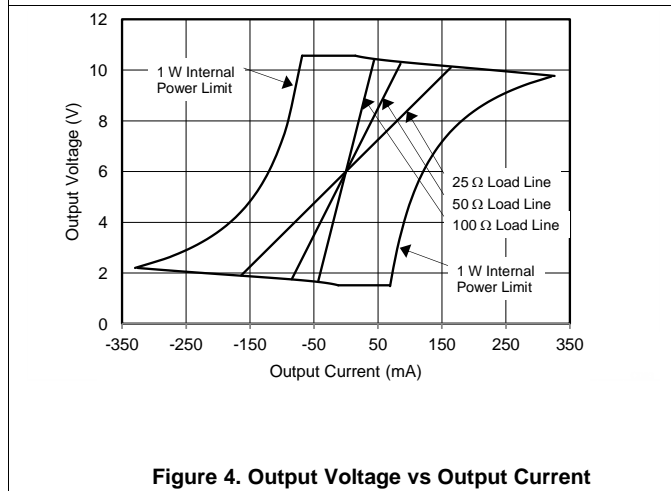


Figure 4. Output Voltage vs Output Current

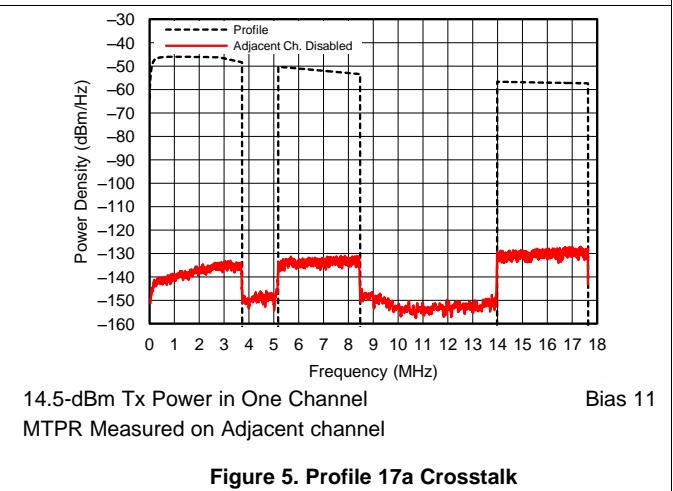


Figure 5. Profile 17a Crosstalk

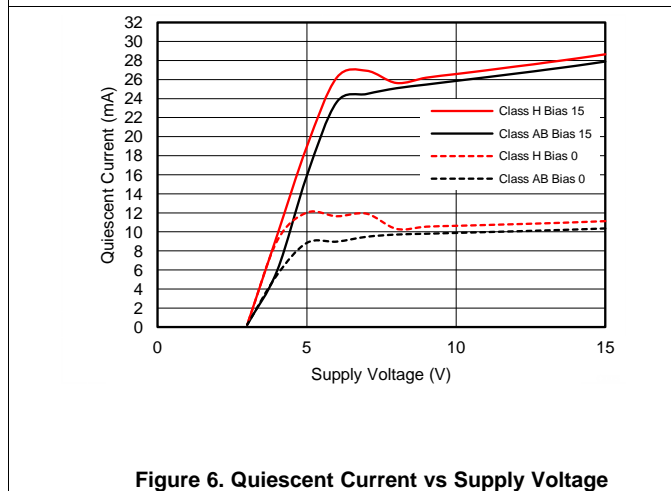


Figure 6. Quiescent Current vs Supply Voltage

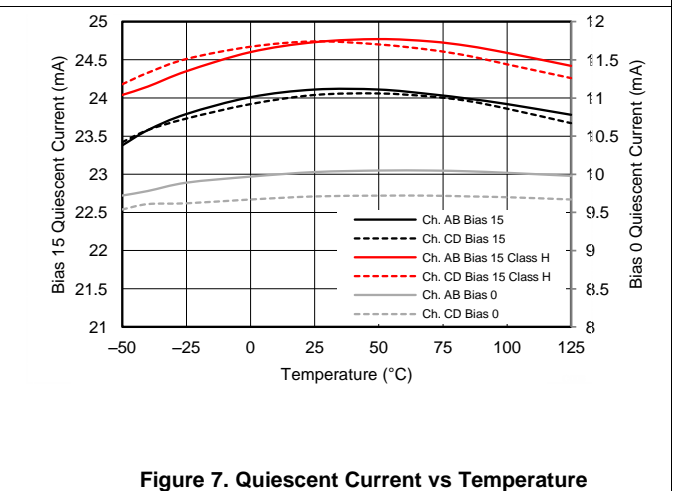
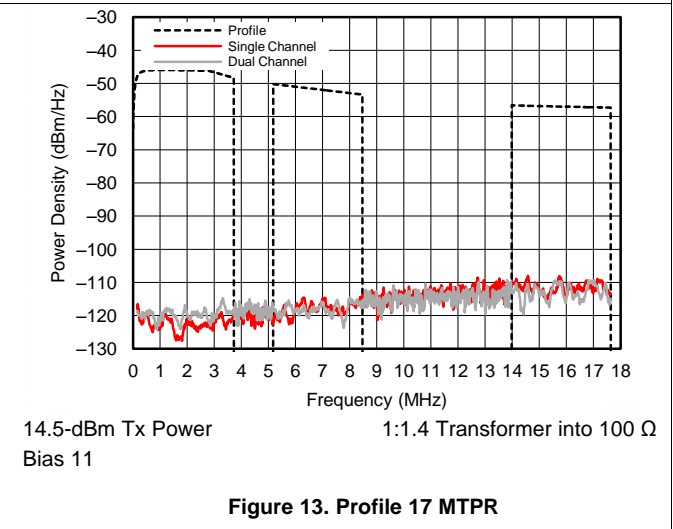
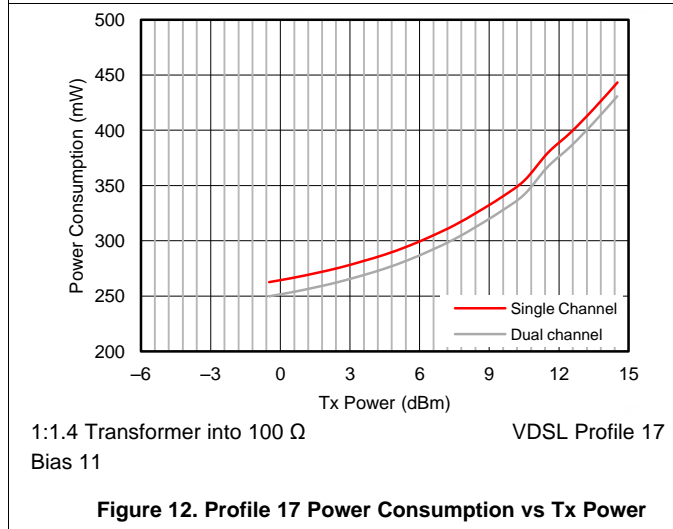
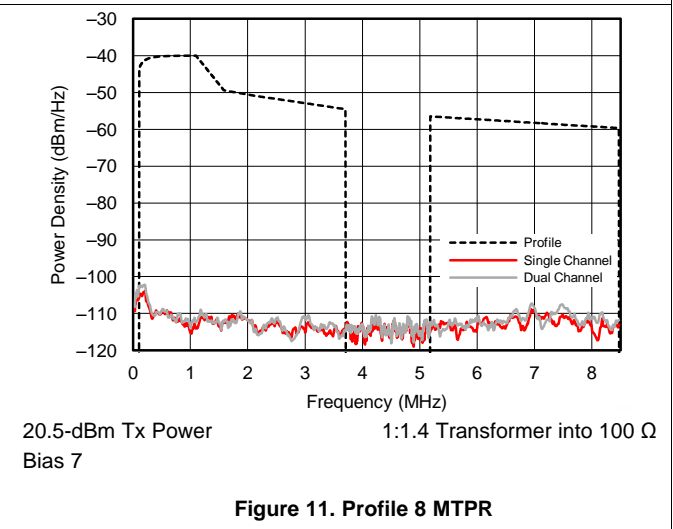
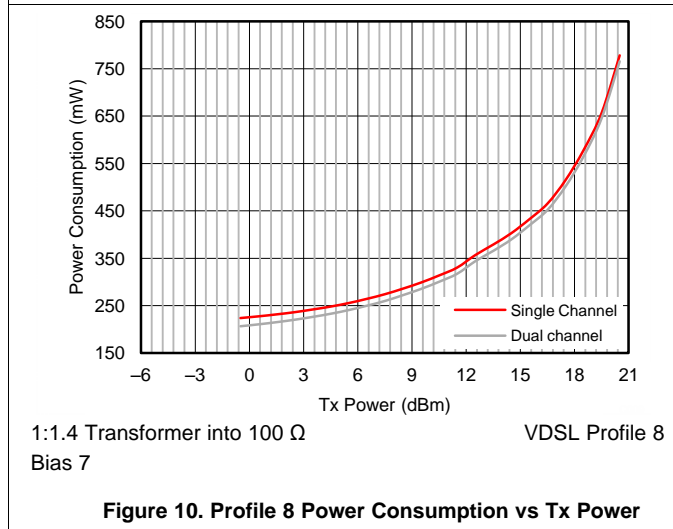
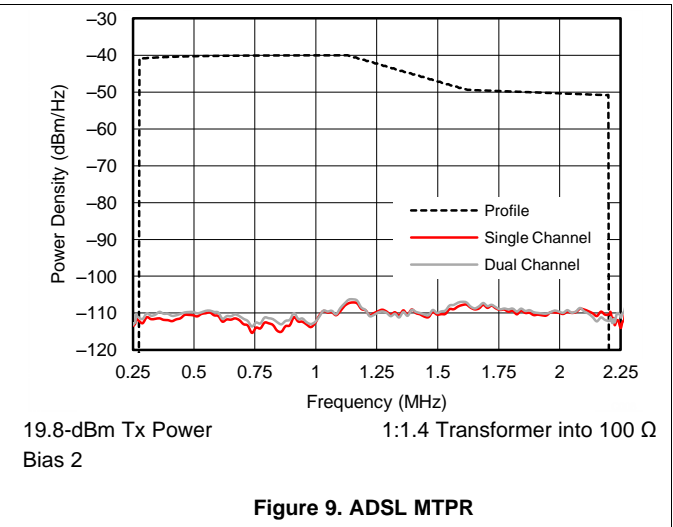
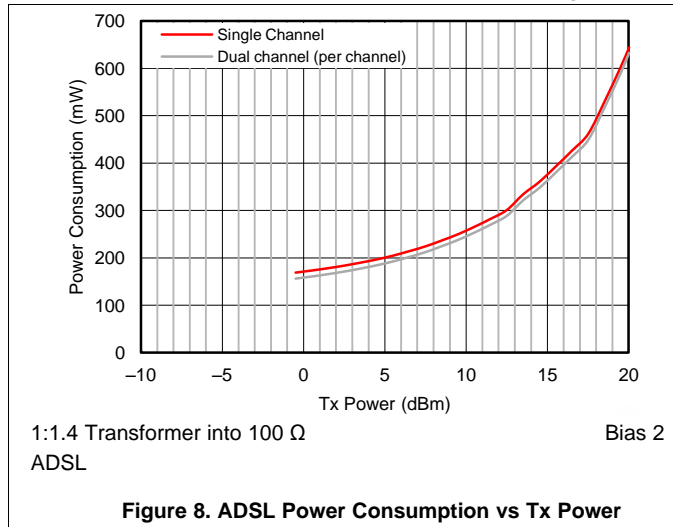


Figure 7. Quiescent Current vs Temperature

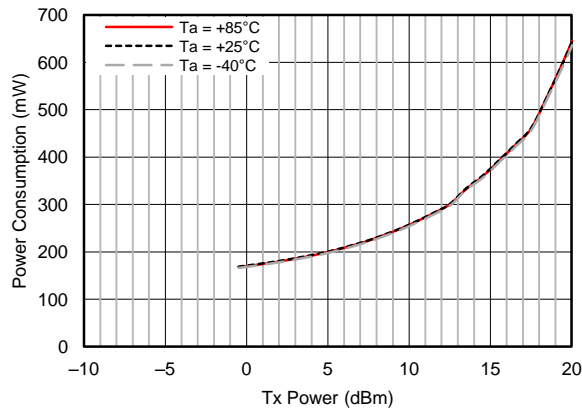
Typical Characteristics (continued)

At  $T_A = 25^\circ\text{C}$ , 1:1.4 transformer, and 10.2- $\Omega$  matching resistance, unless otherwise noted



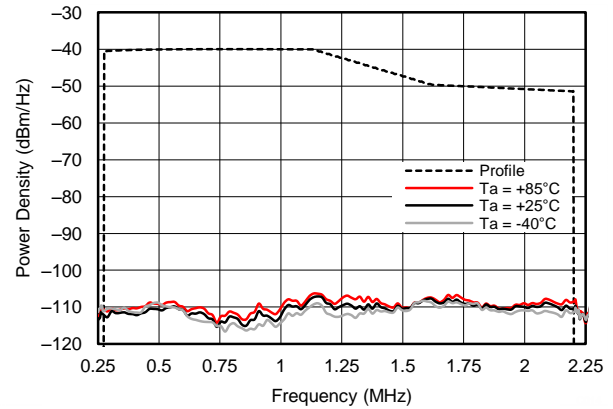
Typical Characteristics (continued)

At  $T_A = 25^\circ\text{C}$ , 1:1.4 transformer, and 10.2- $\Omega$  matching resistance, unless otherwise noted



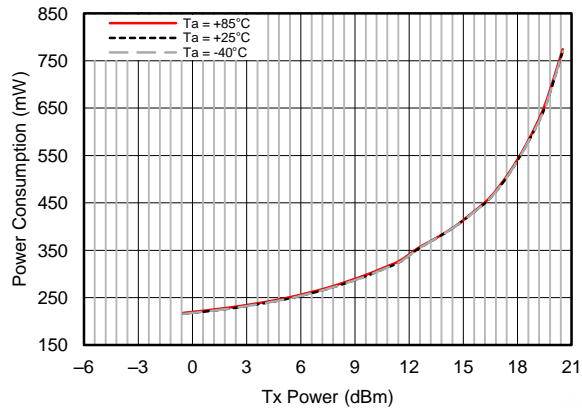
1:1.4 Transformer into 100  $\Omega$  Bias 2  
ADSL

Figure 14. Single-Channel ADSL Power Consumption vs Temperature



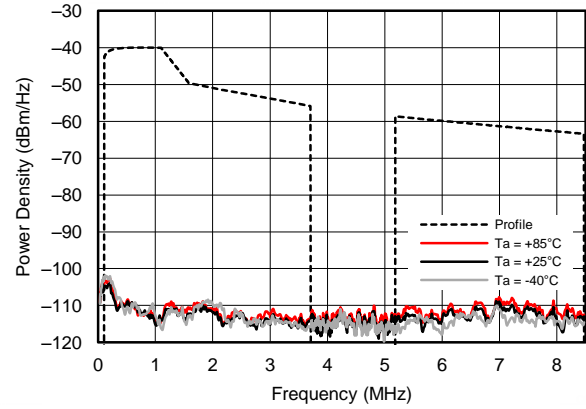
19.8-dBm Tx Power 1:1.4 Transformer into 100  $\Omega$   
Bias 2

Figure 15. Single-Channel ADSL MTPR vs Temperature



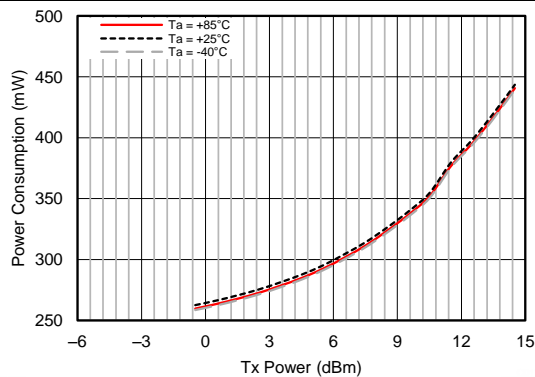
1:1.4 Transformer into 100  $\Omega$  VDSL Profile 8  
Bias 7

Figure 16. Single-Channel Profile 8 Power Consumption vs Temperature



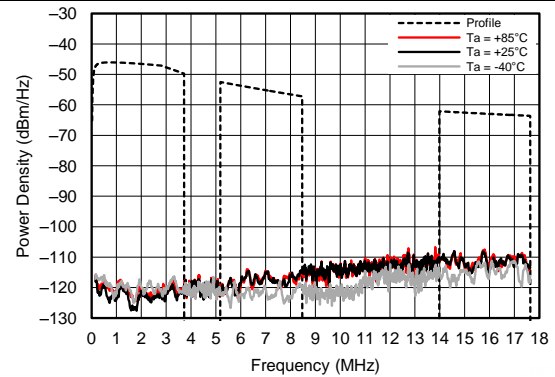
20.5-dBm Tx Power 1:1.4 Transformer into 100  $\Omega$   
Bias 7

Figure 17. Single-Channel Profile 8 MTPR vs Temperature



1:1.4 Transformer into 100  $\Omega$  VDSL Profile 17  
Bias 11

Figure 18. Single-Channel Profile 17 Power Consumption vs Temperature

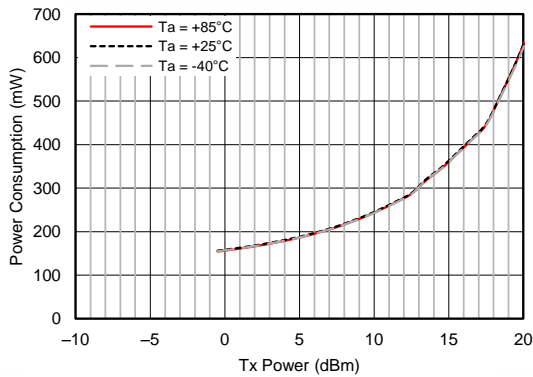


14.5-dBm Tx Power 1:1.4 Transformer into 100  $\Omega$   
Bias 11

Figure 19. Single-Channel Profile 17 MTPR vs Temperature

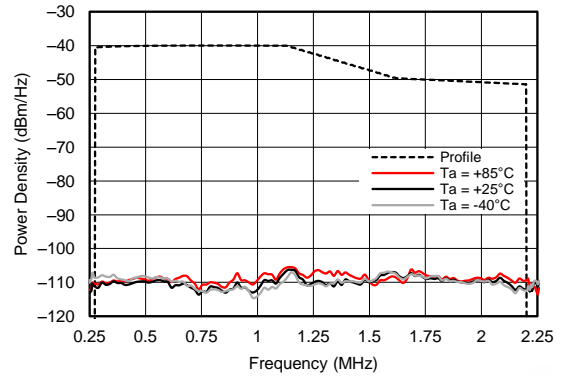
**Typical Characteristics (continued)**

At  $T_A = 25^\circ\text{C}$ , 1:1.4 transformer, and 10.2- $\Omega$  matching resistance, unless otherwise noted



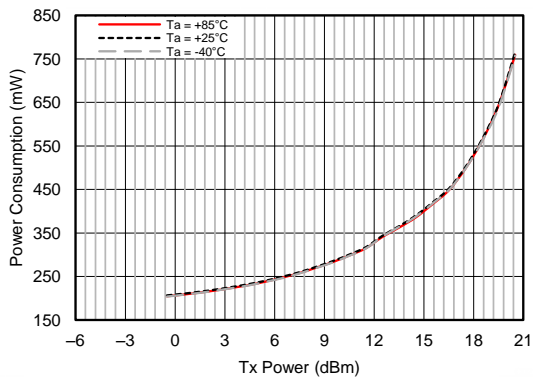
1:1.4 Transformer into 100  $\Omega$  Bias 2  
ADSL Per Channel

**Figure 20. Dual-Channel ADSL Power Consumption vs Tx Power**



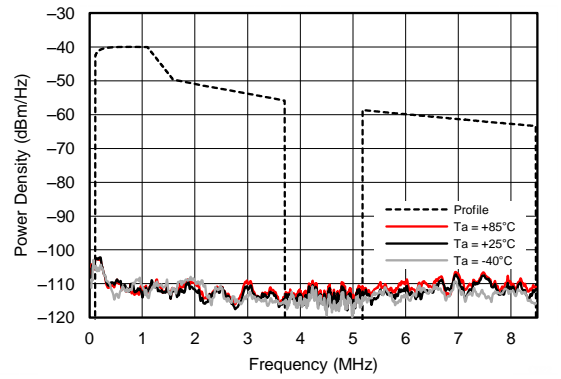
19.8-dBm Tx Power 1:1.4 Transformer into 100  $\Omega$   
Bias 2

**Figure 21. Dual-Channel ADSL MTPR vs Temperature**



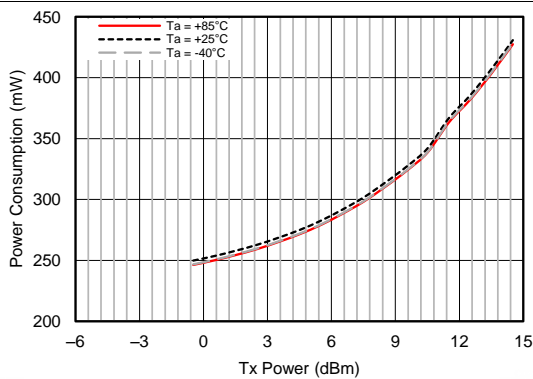
1:1.4 Transformer into 100  $\Omega$  Bias 7  
VDSL Profile 8 Per Channel

**Figure 22. Dual-Channel Profile 8 Power Consumption vs Temperature**



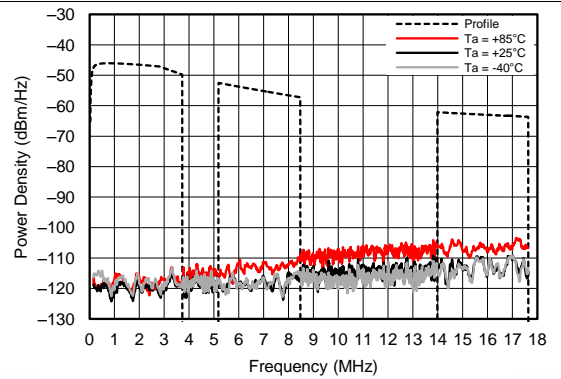
20.5-dBm Tx Power 1:1.4 Transformer into 100  $\Omega$   
Bias 7

**Figure 23. Dual-Channel Profile 8 MTPR vs Temperature**



1:1.4 Transformer into 100  $\Omega$  Bias 11  
VDSL Profile 17 Per Channel

**Figure 24. Dual-Channel Profile 17 Power Consumption vs Temperature**



14.5-dBm Tx Power 1:1.4 Transformer into 100  $\Omega$   
Bias 11

**Figure 25. Dual-Channel Profile 17 MTPR vs Temperature**

Typical Characteristics (continued)

At  $T_A = 25^\circ\text{C}$ , 1:1.4 transformer, and 10.2- $\Omega$  matching resistance, unless otherwise noted

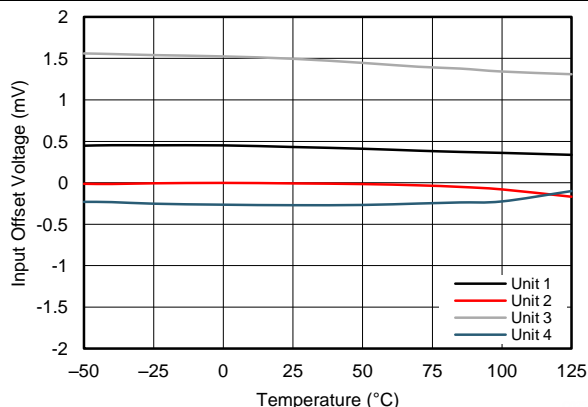


Figure 26. Input Offset Voltage vs Temperature

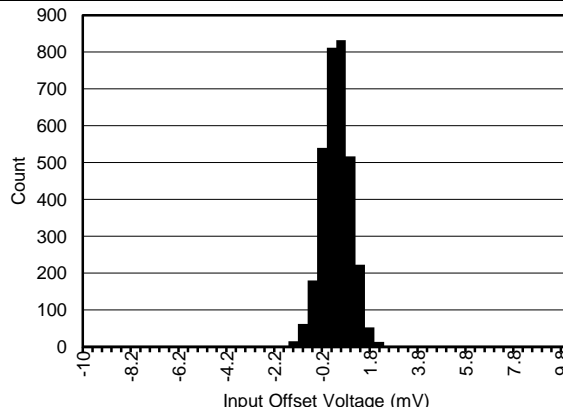
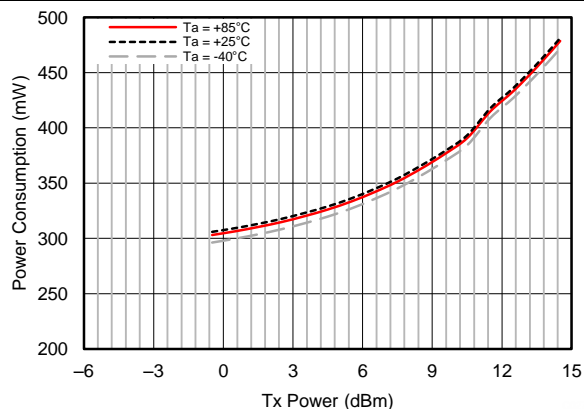
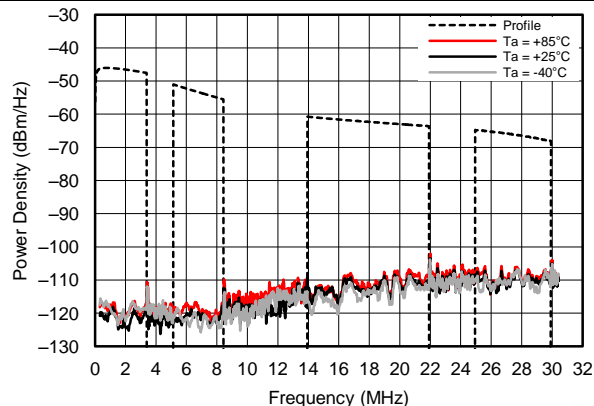


Figure 27. Input Offset Voltage Histogram



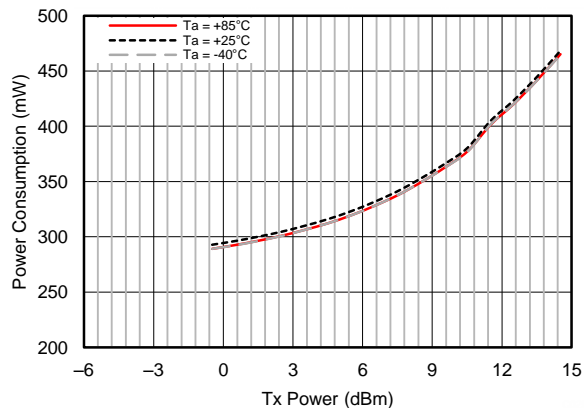
1:1.4 Transformer into 100  $\Omega$  Bias 15  
VDSL Profile 30

Figure 28. Single-Channel Profile 30 Power Consumption vs Temperature



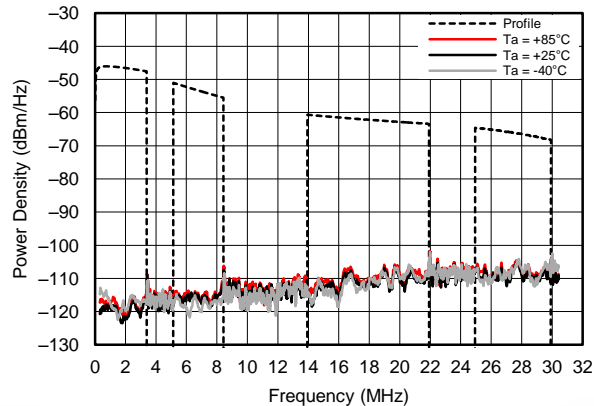
14.5-dBm Tx Power Bias 15  
1:1.4 Transformer into 100  $\Omega$

Figure 29. Single-Channel Profile 30 MTPR vs Temperature



Per Channel

Figure 30. Dual-Channel Profile 30 Power Consumption vs Temperature



14.5-dBm Tx Power Bias 15  
1:1.4 Transformer into 100  $\Omega$

Figure 31. Dual-Channel Profile 30 MTPR vs Temperature

## 7 Detailed Description

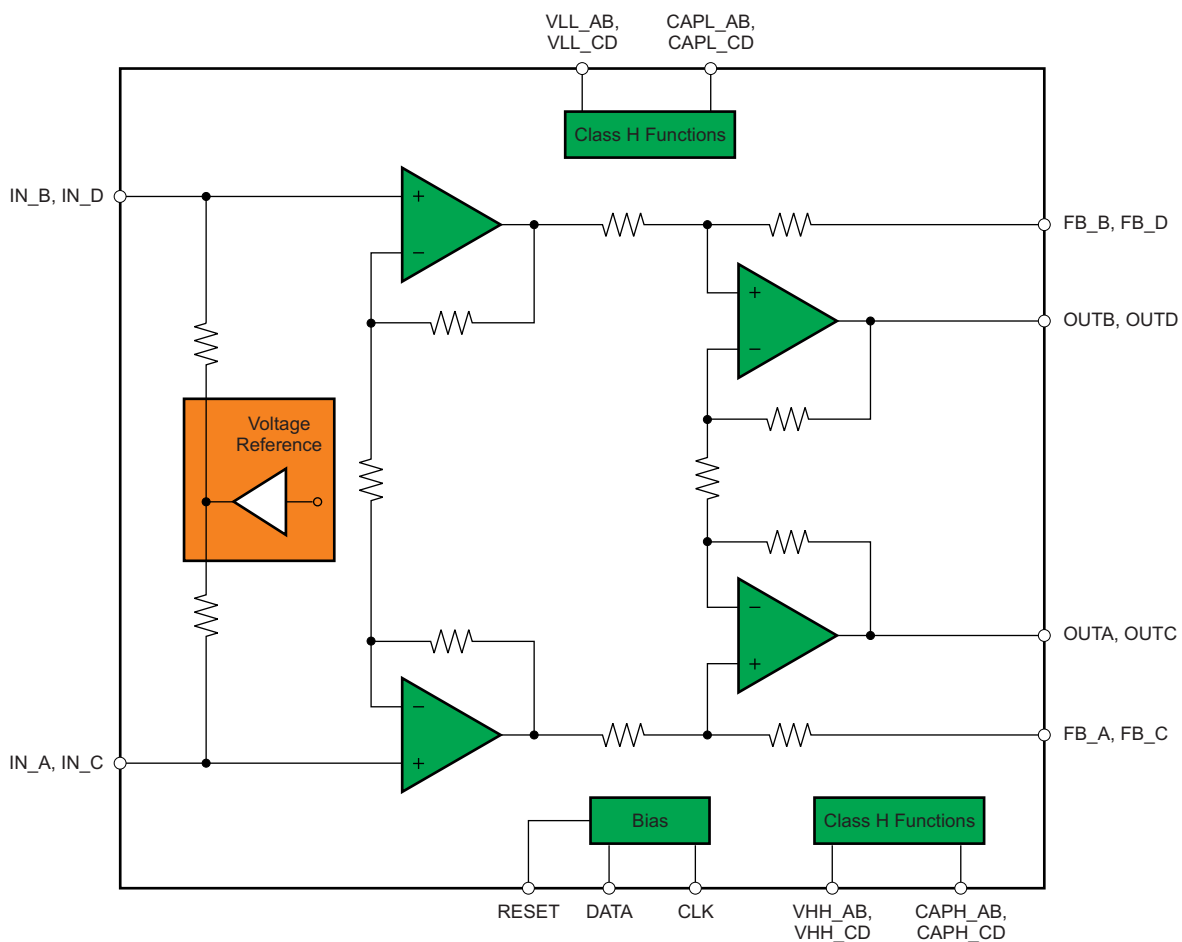
### 7.1 Overview

The THS6226A class H line driver provides exceptional ac performance in conjunction with wide output voltage swing. The class H operation allows voltage swings to exceed the power supply for short intervals limited only by the charge in the capacitor. In class AB mode, the device is capable of driving a 100- $\Omega$  load from +1.8 V to +10.2 V. In class H mode, under the same conditions, the output voltage range becomes an impressive –5.5 V to +17.5 V, or 46  $V_{PP}$  differentially with the capacitor fully charged.

The *Functional Block Diagram* section shows a fully-differential, noninverting amplifier configuration with active impedance. In this configuration, the 10.2- $\Omega$  matching resistor appears through the transformer as 100  $\Omega$ , minimizing reflection on the line. This active impedance scheme also minimizes transmission losses, as compared to passive termination. Device gain is fixed and is equal to 19 V/V from the input to the output of the amplifier ( $IN_{AB/CD}$  to  $OUT_{AB/CD}$ ), not including the transformer-turn ratio or the termination loss.

To simplify the implementation as well as to provide design flexibility, the device contains an integrated mid-supply buffer that provides the correct biasing to the amplifier core without requiring any external components. Also present is a two-pin serial interface that provides exceptional design flexibility and allows minimal power consumption for each xDSL profile.

### 7.2 Functional Block Diagram



### 7.3 Feature Description

The device incorporates several hardware and functionality features: a high output current line driver, a charge pump, a voltage reference, a logic circuit, an active impedance, and a RESET pin. The device has two ports. Each port consists of a high output current line driver, a charge pump, and a reference voltage. Common circuits are the RESET feature and the logic circuit.

#### 7.3.1 High Output Current Line Driver

The main purpose for the device is to provide a high output current into a heavy load. For the THS6226A, with its xDSL application targeted, the load is typically 100  $\Omega$  and currents as high as 400 mA are supported with excellent linearity. The core of the line driver is a class AB amplifier providing both good efficiency and high current drive capability. The high output line driver is the core of the device and any external circuit interface is located on both the device inputs and output.

#### 7.3.2 Charge Pump

The class H functionality of the device is brought on by the integration of a charge pump. The charge pump is a power-supply function to the line driver. The role of the charge pump is to vary the power supply from (12 V / GND) to (20 V / –8 V) and allow the line driver to support high peak to average ratio (PAR) signals while minimizing power consumption and maintaining excellent linearity. The charge pump is controlled externally by the  $V_{H\_EN}$  pin. A logic high on the  $V_{H\_EN}$  pin results in the power supply of the class AB line driver going to (20 V / –8 V), while a logic low on the  $V_{H\_EN}$  pin results in normal operation under the (12 V / GND) supplies.

#### 7.3.3 Voltage Reference

An internal voltage reference provides the device common-mode input and output voltage.

#### 7.3.4 Logic

The DATA and CLK pins allow access to the internal logic circuit implemented in the device. This logic circuit allows each channel to either be programmed individually for quiescent current, turn the charge pump on or off, disable the main amplifier, or select the line termination mode. For more information on programming, refer to the [Programming](#) section.

#### 7.3.5 Active Impedance

The line driver incorporates the positive feedback path to provide the termination to the load. For the device, the synthesis factor implemented is 5.

#### 7.3.6 RESET Pin

The RESET pin provides a quick and easy way to disable the two ports immediately if a fault condition on the line occurs.

### 7.4 Device Functional Modes

There are several functional modes for the device. These functional modes can be accessed with the CLK and DATA pins. Each main line driver quiescent current can be set to 16 different bias modes: bias 0 through bias 15. Additionally, the line driver and class H feature can be controlled to have the following configuration:

- Class AB mode is the main line driver by itself. The output voltage is limited by the (12 V / GND) power-supply rails. The quiescent current is then set by four bits.
- Class H mode is the main line driver used in conjunction with the class H feature. The output voltage is limited by the (20 V / –8 V) internally-generated power-supply rails. The quiescent current of the main line driver is set by four bits, as in class AB mode.
- Line termination mode is the powered-down mode for the line driver. This mode maintains line termination but has reduced linearity performance.
- Disabled mode.

For more information on these mode, refer to the [Programming](#) section.

## 7.5 Programming

### 7.5.1 Programming the Device

Programming the device is accomplished through a serial interface (pins 4 and 5) and proceeds in the following sequence:

- Two start bits are required (B0 = 0 followed by B1 = 1).
- B2 through B9 are used to program the device. (Table 1 lists the bit descriptions.)
- B10 (described in Table 2) is the parity bit that controls whether the word is loaded or not.
- B11 is the stop bit and must be set to B11 = 1.

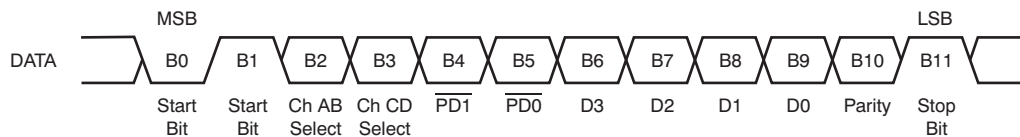
Figure 32 shows the required sequence.

**Table 1. DATA Sequence**

PARAMETER	DESCRIPTION
B0, B1	Start bits
B2, B3	Channel select
B4, B5	Power-down features
B6-B9	Quiescent current setting
B10	Parity bit
B11	Stop bit

**Table 2. Parity Bit**

B10	ODD PARITY BIT
0	For an odd number of high bits in B2 to B9, set B10 to 0
1	For an even number of high bits in B2 to B9, set B10 to 1



**Figure 32. DATA Description**



## 7.5.2 Quiescent Current

The device quiescent current is dissipated in two main device modules: the class AB and the charge pump. Bits B4 (PD1) and B5 (PD0) select one of the possible four modes of operation:

1. Class AB mode (charge pump disabled),
2. Class H mode (charge pump enabled),
3. Disable mode, or
4. Line termination mode (maintains line matching, core amplifier at very low bias mode and charge pump disabled for lowest power consumption possible).

Table 3 lists the details on each bit functionality and the approximate quiescent current. The various power modes are shown in Table 3. For all modes, when B6 through B9 are not defined, set B9 = B8 = B7 = B6 = 0 to achieve the lowest power dissipation possible.

**Table 3. Power Modes**

B4 (PD1)	B5 (PD0)	POWER-DOWN MODE	APPROXIMATE $I_Q$ (mA per Port)
0	0	Power-down (B9 = B8 = B7 = B6 = 0)	0.85
0	1	Line termination mode (B9 = B8 = B7 = B6 = 0)	4.4
1	0	Class AB driver $I_Q$ set by B6 to B9, class H disabled	—
1	1	Class AB driver $I_Q$ set by B6 to B9, class H enabled	—

The class AB quiescent current is set by bits B6 to B9, using B4 and B5 for the power-down function and B2 and B3 for channel selection. The approximate quiescent current for the amplifier core is shown in Table 4.

**Table 4. Class AB Quiescent Current**

BIAS	B6 (D3)	B7 (D2)	B8 (D1)	B9 (D0)	QUIESCENT CURRENT SETTING	APPROXIMATE $I_Q$ (mA per Port)
0	0	0	0	0		9.4
1	0	0	0	1		10.4
2	0	0	1	0	ADSL2+ mode	11.5
3	0	0	1	1		12.5
4	0	1	0	0		13.6
5	0	1	0	1		14.6
6	0	1	1	0		15.7
7	0	1	1	1	Profile 8b mode	16.7
8	1	0	0	0		17.8
9	1	0	0	1		18.8
10	1	0	1	0		19.8
11	1	0	1	1	Profile 17a mode	20.8
12	1	1	0	0		21.8
13	1	1	0	1		22.8
14	1	1	1	0		23.8
15	1	1	1	1		24.8

Channel selection is shown in [Table 5](#). Each channel can be programmed independently, or together if both B2 and B3 are set to 1.

**Table 5. Channel Selection**

B2 (Channel AB)	B3 (Channel CD)	CHANNEL SELECT
0	0	Bits B4 to B9 are ignored
0	1	Channel B programmed with B4 to B9
1	0	Channel A programmed with B4 to B9
1	1	Channels A and B programmed with B4 to B9

At startup, the internal register is set as shown in [Figure 33](#).

**Figure 33. Internal Register**

7	6	5	4	3	2	1	0
Ch. AB Select (B2)	Ch. CD Select (B3)	$\overline{PD1}$ (B4)	$\overline{PD0}$ (B5)	D3 (B6)	D2 (B7)	D1 (B8)	D0 (B9)
W	W	W	W	W	W	W	W

LEGEND: W = Write

In this condition, the total quiescent power dissipation is 10.2 mW per port on a +12-V supply.

## 8 Applications and Implementation

### 8.1 Application Information

The device is a dual-port, very-high-bit-rate digital subscriber line (VDSL), class H line driver. Typically, the signal is generated by a high-speed digital-to-analog converter (DAC). The device drives a twisted pair.

The digital subscriber line (DSL) system is ac-coupled as it transmits information above the audio band. On the input of the line driver, this ac-coupling translates into the series capacitors to isolate the dc voltage coming from the DAC output common-mode voltage. On the output, a transformer is used to help isolate the 48V present between tip and ring of the telephone line.

The transformer can be set to any useful ratio. In practice, the transformer-turn ratio is set between 1:1 and 1:1.4 for the device. As mentioned in the [Feature Description](#) section, the active impedance synthesis factor is 5. This synthesis factor means that the termination resistor is 1/5th of the load impedance reflected to the transformer secondary. Thus, the correct termination can be selected based on the transformer-turn ratio.

Note that the resulting load detected by the amplifier may affect the amplifier linearity or output voltage swing capabilities.

### 8.2 Typical Application

The typical application circuit for this application is shown in [Figure 34](#).

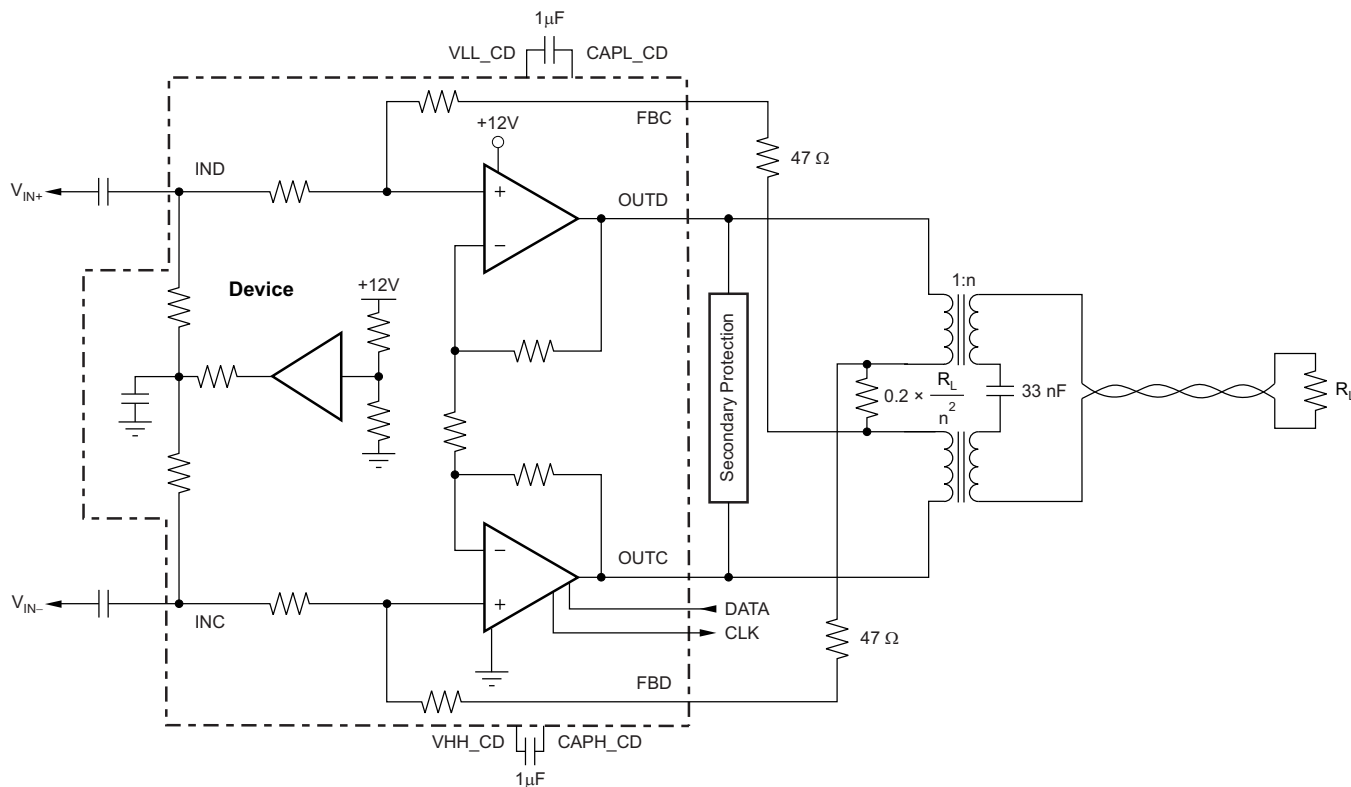


Figure 34. Typical VDSL Line Driver Circuit Configuration

## Typical Application (continued)

### 8.2.1 Design Requirements

**Table 6. Design Requirements**

DESIGN REQUIREMENT	CONDITION
AC-coupling capacitors	0.1 $\mu$ F
Synthesis factor	5
Output transformer ratio	1:1.4
Surge protection circuit	Not shown

### 8.2.2 Detailed Design Procedure

The input capacitor forms a high-pass filter with the device input impedance. This pole must be set at a frequency low enough to not interfere with the desired signal.

The output transformer can be changed to any transformer-turn ratio. Note that the load is expected to be a transmission line with 100- $\Omega$  characteristic impedance. Referred to the transformer secondary, the load detected by the amplifier is  $1 / n^2$  with 1:n being the transformer-turn ratio.

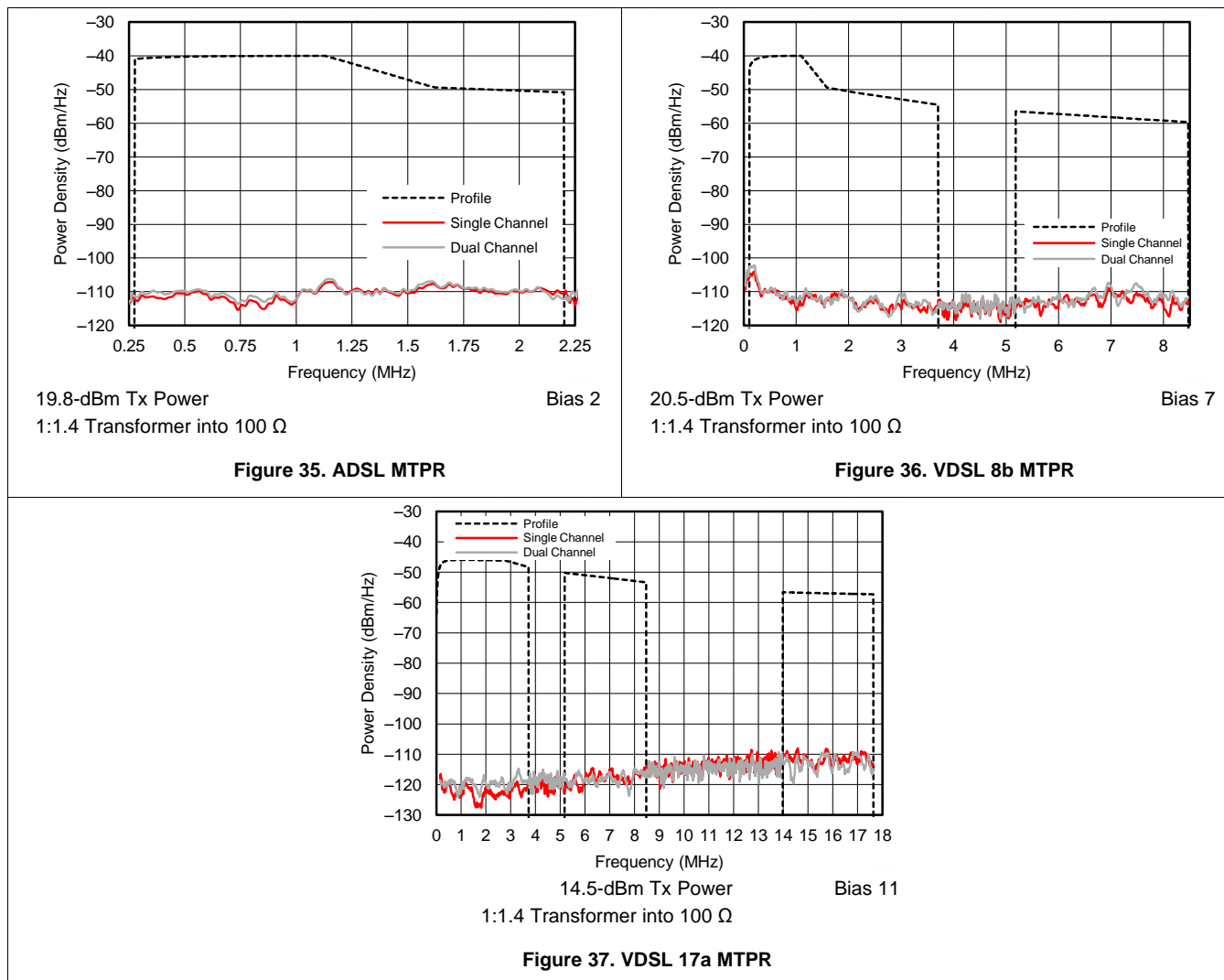
Practical limitations force the transformer-turn ratio to be between 1.4:1 and 1:2. At the lighter load detected by the amplifier (1.4:1), the voltage swing is limited by the class H and the maximum achievable swing of the amplifier. At the heaviest load (1:2), the voltage swing is limited by the current drive capability of the amplifier. To satisfy the synthesis impedance factor and the loading, the series resistance ( $R_S$ ) can be set to  $R_S = R_L / 5 = 100 \Omega / (5 \times n^2)$ .

For the charge pump, consider the thermal characteristic of the capacitor (X7R, X5R, or Y5V can be used for the charge pump).

For the power-supply bypass, consider using only X7R or X5R because of the better stability of these materials over temperature.

For surge protection, consider adding 47- $\Omega$  resistors in series on the positive feedback path. The secondary protection is also normally added after the series resistance on the secondary transformer.

### 8.2.3 Application Curves



### 8.3 Initialization Set Up

After the initial power-up and prior to sending any words to program the device, TI recommends sending a string of twelve 1s (111111111111) to ensure that the state machine is initialized.

## 9 Power Supply Recommendations

As a result of large recharge current flowing in and out of the four charge pump capacitors during charge pump discharge and recharge events, TI recommends placing bypass capacitors that are at least equal in value to the charge pump capacitor close to each supply voltage pin. A minimum of 2-μF bypass capacitors for each channel are required to minimize any transient appearing on the power supply because both positive and negative charge pump 1-μF bypass capacitors are recharged on the +12-V supply.

## 10 Layout

### 10.1 Layout Guidelines

Achieving optimum performance with a high-frequency amplifier such as the THS6226A requires careful attention to board layout parasitics and external component types. Recommendations that optimize performance include:

- a. **Minimize parasitic capacitance** to any ac ground for all signal I/O pins. Excessive parasitic capacitance on the inverting input pin can cause instability. In the line driver application, the parasitic capacitance forms a pole with the load detected by the amplifier and may reduce the effective bandwidth of the application circuit, thus leading to degraded performance. To reduce unwanted capacitance, open a window around the signal I/O pins in all ground and power planes around those pins. Otherwise, make sure that ground and power planes are unbroken elsewhere on the board.
- b. **Minimize the distance** (< 0.25") from the power-supply pins to high-frequency 0.1- $\mu$ F decoupling capacitors. At the device pins, make sure that the ground and power-plane layout are not in close proximity to the signal I/O pins. Avoid narrow power and ground traces to minimize inductance between the pins and decoupling capacitors. Always decouple the power-supply connections with these capacitors. An additional low ESR supply decoupling capacitor ( $\geq 2 \mu$ F, X7R or X5R) to ground is necessary to provide a transient current during the charge pump capacitors recharge.
- c. **Careful selection and placement of external components preserves the high-frequency performance of the device.** Use very low reactance type resistors. Surface-mount resistors function best and allow a tighter overall layout. Metal-film or carbon composition, axially-leaded resistors also provide good high-frequency performance. Again, keep the leads and printed circuit board traces as short as possible. Never use wire-wound type resistors in a high-frequency application.
- d. **Connections to other wideband devices** on the board can be made with short, direct traces or through onboard transmission lines. For short connections, consider the trace and the input to the next device as a lumped capacitive load. Use relatively wide traces (50 mils to 100 mils), preferably with ground and power planes opened up around them.
- e. **Do not socket a high-speed part such as the THS6226A.** The additional lead length and pin-to-pin capacitance introduced by the socket can create an extremely troublesome parasitic network that makes achieving a smooth, stable frequency response almost impossible. Best results are obtained by soldering the device onto the board.

## 10.2 Layout Example

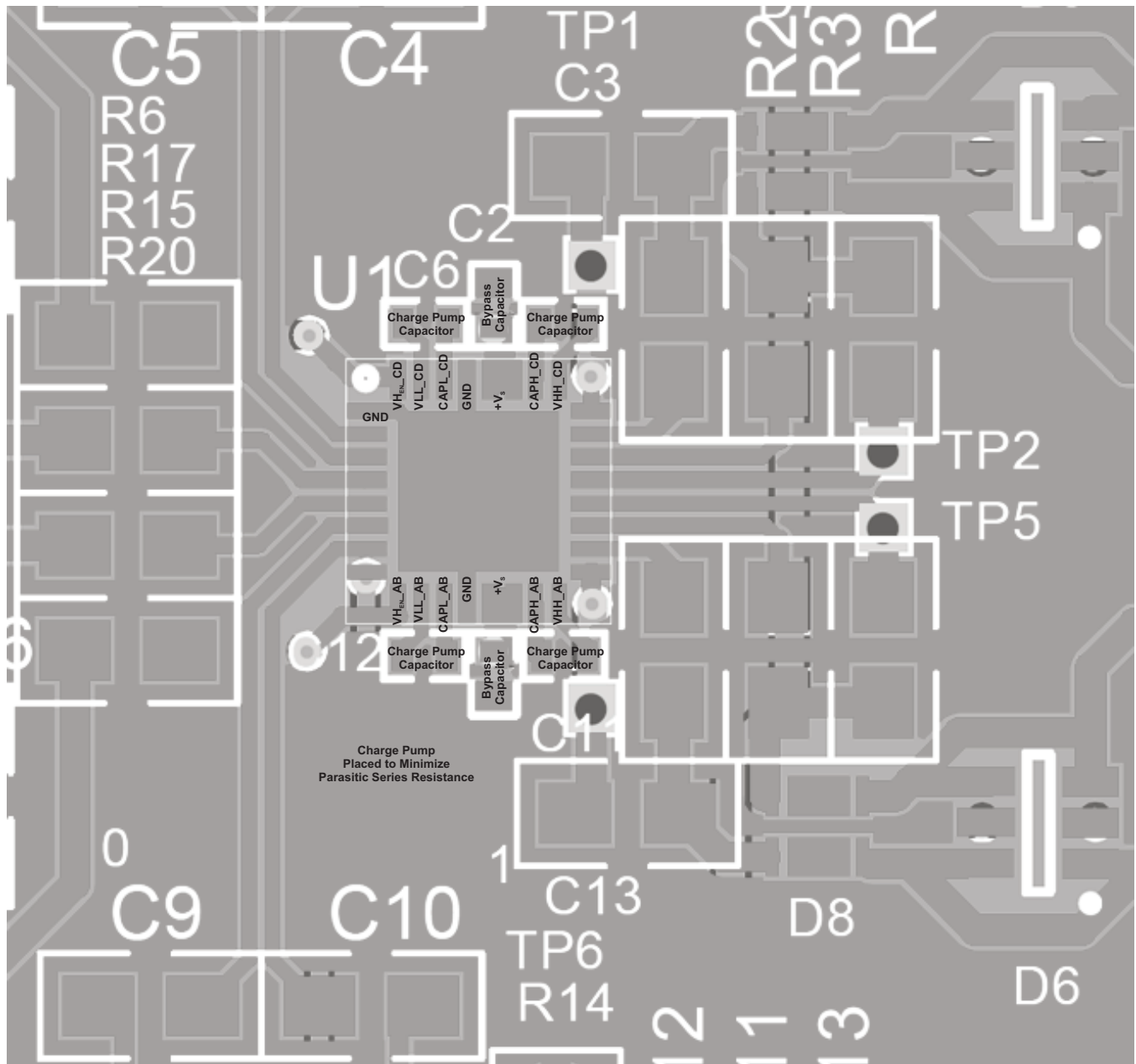


Figure 38. Layout Example

## 11 Device and Documentation Support

### 11.1 Documentation Support

#### 11.1.1 Related Documentation

For related documentation see the following:

- *PowerPAD™ Thermally Enhanced Package*, [SLMA002](#)

### 11.2 Trademarks

PowerPAD is a trademark of Texas Instruments, Inc.  
All other trademarks are the property of their respective owners.

### 11.3 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### 11.4 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms and definitions.

## 12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical packaging and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.



**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
THS6226AIRHBR	LIFEBUY	VQFN	RHB	32	3000	RoHS & Green	NIPDAU	Level-3-260C-168 HR	-40 to 85	HS6226A IRHB	
THS6226AIRHBT	LIFEBUY	VQFN	RHB	32	250	RoHS & Green	NIPDAU	Level-3-260C-168 HR	-40 to 85	HS6226A IRHB	

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

**Important Information and Disclaimer:**The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.



**TAPE AND REEL INFORMATION**

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
THS6226AIRHBR	VQFN	RHB	32	3000	330.0	12.4	5.3	5.3	1.1	8.0	12.0	Q2
THS6226AIRHBT	VQFN	RHB	32	250	180.0	12.4	5.3	5.3	1.1	8.0	12.0	Q2

**TAPE AND REEL BOX DIMENSIONS**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
THS6226AIRHBR	VQFN	RHB	32	3000	346.0	346.0	33.0
THS6226AIRHBT	VQFN	RHB	32	250	210.0	185.0	35.0

## GENERIC PACKAGE VIEW

**RHB 32**

**VQFN - 1 mm max height**

5 x 5, 0.5 mm pitch

PLASTIC QUAD FLATPACK - NO LEAD



Images above are just a representation of the package family, actual package may vary.  
Refer to the product data sheet for package details.

4224745/A



4223442/B 08/2019

NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.

# EXAMPLE BOARD LAYOUT

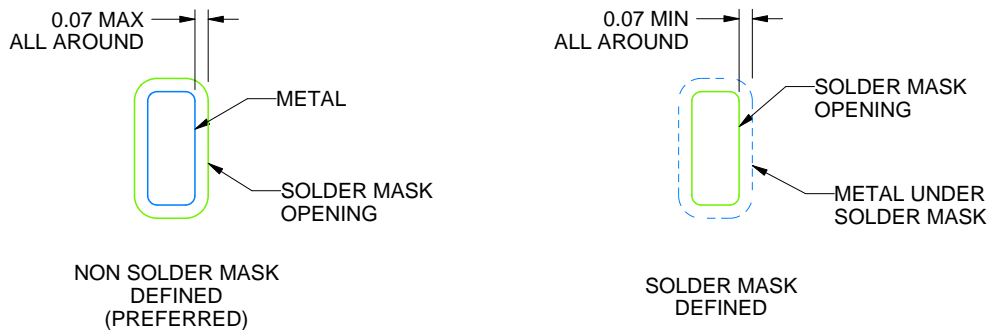
RHB0032E

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



LAND PATTERN EXAMPLE  
SCALE:18X



SOLDER MASK DETAILS

4223442/B 08/2019

NOTES: (continued)

- This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 ([www.ti.com/lit/slua271](http://www.ti.com/lit/slua271)).
- Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.

# EXAMPLE STENCIL DESIGN

RHB0032E

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



**SOLDER PASTE EXAMPLE**  
 BASED ON 0.125 mm THICK STENCIL

EXPOSED PAD 33:  
 75% PRINTED SOLDER COVERAGE BY AREA UNDER PACKAGE  
 SCALE:20X

4223442/B 08/2019

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.



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